

Experimental Analysis of Performance Improvement of a Modified Vapour Absorption System (VAS-GAX) for Cooling Applications



Suyambazhahan Sivalingam^{1*}, Sakthivel Thirumalai Gopal², Vivek Pandey¹, Mohanram Parthiban¹

¹ Department of Mechanical Engineering, School of Mechanical, Chemical and Materials Engineering, Adama Science and Technology University, Adama 1888, Ethiopia

² Saveetha School of Engineering, SIMATS Deemed University, Chennai, Tamil Nadu 600077, India

Corresponding Author Email: suyamiitm@gmail.com

<https://doi.org/10.18280/ijht.390623>

ABSTRACT

Received: 3 November 2021

Accepted: 27 December 2021

Keywords:

VAS-GAX system, cooling applications, COP improvement, saving electrical energy, less environmental harm and lower losses

Experiments on an enhanced “Generator-Absorber-Heat Exchanger” (GAX) Vapour Absorption System (VAS) for cooling purposes were carried out using water-ammonia in present study. The new experimental setup was fabricated using modern and complex technologies for the GAX absorption system which includes tiny heat exchangers, allowing the system to be both compact and efficient. The coefficient of performance (COP) of a system was analyzed for different temperatures of Generator, Condenser, Evaporator and Absorber. The results show that the maximum performance (COP=0.63) is achieved at 25°C Generator temperature. The system has a low carbon footprint because it does not use effluent water or tower electricity and invention enables the recovery of hot air, which may then be used for several drying applications, including agricultural drying, resulting in a fully cascaded system with a three-fold increase in Coefficient of Performance (COP). A modified VAS-GAX absorption system in present analysis be a good fit for high-performance modern cooling applications.

1. INTRODUCTION

The routinely used refrigerants in commercial refrigeration systems are causing several environmental issues. Various refrigerants are frequently used in vapour absorption refrigeration (VAR) and may give an improved option to lessen the environmental impact [1] of hydro chloro fluoro carbons (HCFC), chloro fluoro carbons (CFC) and hydr fluoro carbons (HFC) and maybe replace the vapour compression system (VCR) system. VAR provides several advantages, including lower losses, improved co-efficient of performance (COP), lower power consumption, and reduced environmental impact [2]. The absorption refrigeration system is not employed for commercial applications due to its low performance and thus requires development. Renewable energy is also the only solution for rural areas in distant areas where meeting electricity demand is difficult. VAR is capable of quickly adapting to renewable technologies such as solar photovoltaics and solar thermal systems. It enables rural cold storage even in the most remote areas. The temper Green technology is perfect for preserving tropical agricultural produce at temperatures ranging from 10 to 15°C. The refrigeration process has seen significant technological advancements, but the basics of the process remain same. As a part of the ongoing search for newer technologies in research, valuable alternatives to the standard vapour-compression mechanism identified as typical vapour-compression system. In this work, a novel operating model of an alternate refrigeration system is built in a simple VCR system utilizing modern and complex technologies to improve system efficiency, minimize electrical energy consumption, and lessen environmental harm.

Srivastava et al. [3] performed a study on uses of renewable energy sources such as sun, wind, and geothermal, the NH₃-H₂O Absorption Refrigeration System offers a low-cost alternative to existing systems. The use of solar energy to create refrigeration systems has the most negligible impact on the environment and humans.

Boudéhenn et al. [4] developed and compared the performances of ammonia-water absorption chillers with cooling capacities of 5kW and 100 kW. The chillers were powered by solar energy or waste heat. In addition, a chilled cooling capacity of 100 kW was developed to produce ice by delivering a cooling effect at temperatures suitable for air conditioning. They showed that their design enabled quick start-up operation and adapted quickly to low/partial loads. Osta-Omar and Micallef [5] examined and optimized the vapour solution interface area on a miniature lithium bromide VARS, for various absorption rates. The miniature device could have applications for electronics cooling devices at miniature level. The system was equipped with an adiabatic absorber. The solution thickness was found to have the least effect on the absorption rate, with an optimum vapour solution interface area of 140 cm².

Ramesh et al. [6] experimentally evaluated the performance of a shell and coil heat exchanger (SHX), which was a component of an NH₃-H₂O based VAR system. The SHX was explored for the heat transfer co-efficient (HTC) on the coil, which would significantly influence the total HTC and shape of the SHX. They found a shell side heat transfer coefficient of 510 to 650 W/m²K and a heat exchanger efficacy of 0.84 to 0.9 for the studied conditions. Jain et al. [7] investigated a 100 kW, combined vapour compression absorption integrated refrigeration system (VCAIRS) using low-grade, waste heat.

The system was compared to a vapor compression-absorption cascaded refrigeration system (VCACRS), of same capacity. Electricity consumption for VCAIRS was 21.4 percent more than VCACRS. However, electricity consumed was 63% less compared to VCRS. Moreover, the second law effectiveness of VCAIRS, VCACRS, and VCRS were established at 27.9%, 32.73%, and 18.83%, respectively. The VCACRS was found to be comparatively more energy-efficient cooling technology.

Al-Amir and Khudair [8] investigated a branched GAX absorption cycle operating with $\text{NH}_3\text{-H}_2\text{O}$ pair. Under static conditions, the Engineering Equation Solver (EES) software was used for performance analysis. The results showed that when the temperature in the generator and evaporator rises, the mean COP and cooling capacity of the device rose, but as the temperature in the condenser rises, the mean COP and cooling capacity falls. In addition, the split ratio and ammonia content difference significantly impacted chiller absorption. Ponshanmugakumar and Rajavel [9] did experiments on vapour absorption generator. The phase change material (PCM) was used for thermal energy storage system in generator. The generator design was altered to accommodate PCM confinement and an average temperature of 60°C to 80°C for the heat energy available. PCM were made of combinations of paraffin wax, and graphite powder. Furthermore, the storage tank was assessed for thermal energy charging and discharging by changing the material composition.

Talpada and Ramana [10] reviewed the performance improvement of basic VAS with cycle modifications. An absorption refrigeration system must perform well in order to be a viable alternative to vapour compression refrigeration systems. Also, switching to absorption systems improves the efficiency of absorption cooling systems. The employment of a double- and semi-generator heat exchanger solution system improves cooling absorption effectiveness. The combination of compression-absorption and expulsive-absorption cycles improves the cooling performance of the absorption coefficient. Praveen et al. [11] analyzed a Vapor Absorption Refrigeration (VAR) system run with waste heat from an internal combustion (IC) engine's exhaust gas. The exhaust from a 1.5L diesel engine was used. Sage Math 9.0 was used to analyse the VAR system. The heat transmission across various system components was compared with different VAR system temperatures, and the COP examined with varied generator temperatures. The results revealed that as the input temperature rises, the system's performance increased. Lima et al. [12] carried out an updated evaluation of recent advancements and recommendations for improving the operation of absorption refrigeration systems using various working fluids. Because of the low temperature of the ammonia operation, ammonia-water pair is used in air conditioning and industrial processes. Solar energy is used as a source of input to improve the efficiency of absorption cooling systems.

Jain et al. [13] assessed the thermodynamic potentials and related risks of $\text{NH}_3\text{-H}_2\text{O}$ and $\text{H}_2\text{O-LiBr}$ integrated vapour absorption refrigeration (IVARS). Their proposed design keeps an evaporator temperature of 92.1°C at 30°C , which is 51.6°C lower than the required VARS-standard cooling temperature for the same cooling task. This issue is addressed with exergy analyses. Surprisingly, 19.8 percent of the IVARS irreversible loss was proven to be preventable by adjusting the efficiency settings of various IVARS components, whereas the remaining 93.7% was determined to be irreversible. The results showed that IVARS performs better and may be used

with low-temperature waste heat recovery.

Tetemke et al. [14] studied the influence of several design and operation scenarios on the COP of the cooling system which was established through simulation energy. AVAR system employing geothermal energy to provide waste thermal cooling, was investigated. For cooling a drinking water supply, from 37.8°C to 16°C in 16 hours, VARS components were analyzed utilizing mass and energy conservation principles. Furthermore, at an evaporation rate of 103.12 kW, the VAR system could cool 66,000 litres of beverage water. These results show that the evaporation rate varies with time, VAR systems powered by geothermal energy.

As per the above literature, part of the ongoing search for alternative technologies that would use renewable energy sources, valuable alternatives such solar, geothermal, waste heat, are identified as sources for the standard vapour-compression mechanism. The novelty of this paper is, an alternate absorption refrigeration system with a novel design for higher refrigeration effect is developed by building the system into an existing ARS-GAX system, resulting in reduced losses, increased performance, and lower electrical energy consumption.

2. MATERIALS AND METHODS

The Absorption Refrigeration System consist of a pump, an absorber, a generator, a solution heat exchanger, a condenser, a rectifier, a refrigerant heat exchanger and an evaporator. A cooling absorption system using a binary solution of absorbent and refrigerant as a working fluid. The most commonly utilized fluid absorption systems in large buildings or plants for commercial and industrial cooling purposes are ammonia-water and LiBr-water systems. This study will look into a modified ammonia-water absorption cooling GAX system. The American Society of Heating, Refrigeration, and Air Conditioning Engineers (ASHRAE) promotes the design and implementation of HVAC, AV, and conditioning systems. The ASHRAE Handbook goes into great depth about how the two-fluid absorption refrigeration system works.

The system is divided into two pressure limits: one for the generator and one for the evaporator. The high-pressure solution flows via the generator and solution heat exchanger which engrosses heat from the source, and finally the rectifier, which mixes the ammonia and water mixture. After the water content in the ammonia is separated, pure ammonia vapour goes to the condenser. The weak solution is recirculated through the absorber and solution heat exchanger. The refrigerant vapour is condensed into a liquid by losing heat to the surrounding environment via convection in the condenser. The liquid ammonia is further cooled using refrigerant heat exchanger and directed to the evaporator. The refrigerant reaches a temperature below saturation after passing through the rectifier and into the evaporator, and the heat is absorbed by the area to be cooled in the refrigerator, forcing the refrigerant to become vapour. The refrigerant is then sent to the solution heat exchanger, where it absorbs ammonia from the water, and the cycle repeats. The studies were carried out by adjusting the mass flow rate on the generator, condenser, absorber, and evaporator for various specified temperatures and calculating the COP.

The temperature of the remaining coolant reduces by absorbing the coolant vapour, as a result of the "vaporisation process." Simultaneously, the solution becomes diluted as a

result of the higher coolant content absorbed. It is referred to as “the absorption process.” Because of its basic exothermic absorption process, heat must be rejected in the environment to sustain the product’s absorption capacity. By utilizing heat energy, the refrigeration effect can be achieved in a variety of ways. Since the process cannot be finished concurrently, the cooling effect cannot be created continually. As a result, a new GAX cycle is designed that combines these two approaches to increase performance and offer continuous cooling. The COP of an absorption system is obtained from:

$$\begin{aligned}
 &= \frac{COP}{\text{cooling capacity of evaporator}} \\
 &= \frac{\text{heat input to the generator} + \text{work input to the pump}}{Q_e} \quad (1) \\
 &= \frac{Q_g}{Q_g}
 \end{aligned}$$

The pump’s effort is typically neglected in assessments since it is minor concerning the generator’s heat input.

Overall, the absorption cycle performs poorly per unit energy input; however, system waste heat can be used to increase overall energy utilization. Ammonia/water (NH₃/H₂O) systems are typically employed when a lower temperature is required. Each system component is computed and summarized with mass and heat flow rates. The system’s coefficient of performance is calculated for several temperature ranges.

2.1 Ammonia-water single stage absorption refrigeration system

A cooling cycle system consists of a heat exchanger, evaporator, absorber, pump, two flow limits (expansion valve), a heat exchanger solution, a generator, a rectifier, and a condenser. Figure 1 illustrates the layout and flows direction of an ammonia-water single-stage absorption cooling system’s mixing of solution and ammonia vapour. The cycle is separated into two fluxes: one with an ammonia-water mix and one with ammonia vapour. Points (1-6) indicate the ammonium hydroxide solution cycle, whereas “the remaining points reflect the ammonia vapour cycle. The rich solution (1) is pumped through the solution heat exchanger (2) with higher pressure into the generator (3), where heat added to an ammonia-water vapour mixture, while the poor solution (4) is returned to the absorber via solution heat exchanger and flow restrictor (5, 6). The ammonia-water vapour is purified in the rectifier by condensing the water vapour in the combination into a liquid”. The condenser receives both the water liquid and the pure ammonia vapour (7). While flowing through the condenser, ammonia vapour loses heat to the environment and cools into fluid ammonia (8). The ammonia fluid is further cooled by a coolant heat exchanger (9) before passing through a flow-limiting system (10) with a quick pressure drop, where it evaporates since the new pressure is lower than its saturation. At the new pressure and temperature, ammonia become saturated vapour. The temperature of the components is always lower than the optimal temperature. The evaporator collects the heat from the refrigerator and directs the saturated ammonia vapour to it. The ammonia vapour (11) is absorbed into the water by the absorber after passing through the heat exchanger a second time (12). To restart the process, the generator delivers the ammonia-water vapour mixture to the rectifier (13), and the rectifier sends the water liquid back to the generator (14).

Several fluids are being studied, and the potentiality of the

same was checked. The low circulation rate of the working fluid and low generator temperature are the challenges in making VAS – GAX employable. Recent works are reported on the binary working fluids for the absorption cycles.

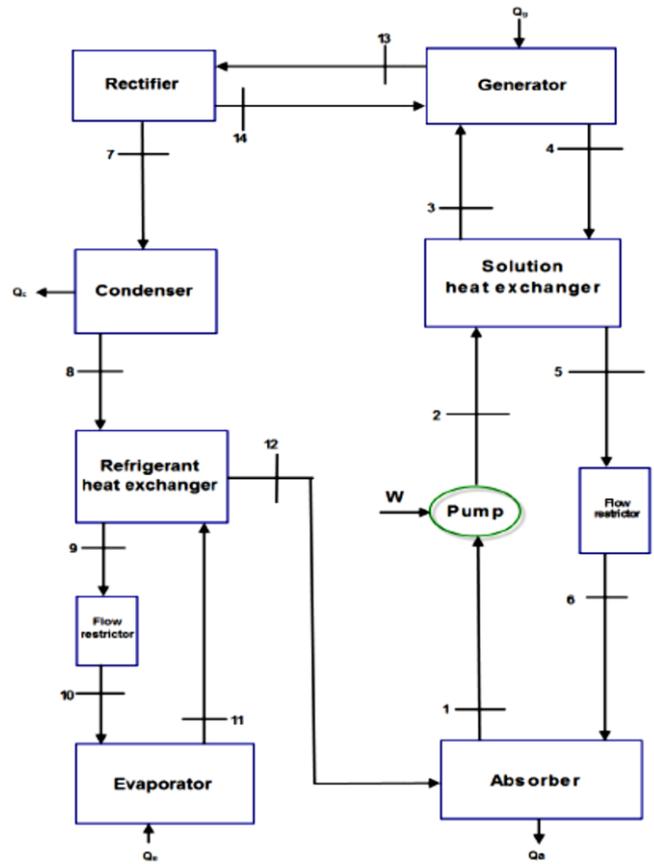


Figure 1. Ammonia water single stage absorption refrigeration system

2.2 LiBr/water absorption refrigeration systems

There are two significant advantages of using “LiBr/water” for absorption refrigeration systems: LiBr is a non-volatility absorbent (no need for a rectifier) with an unusually high heat of vaporisation of water (refrigerant). Low-temperature applications, however, are limited to that above 0°C due to the usage of water as a refrigerant. The system must be run under a vacuum because the refrigerant used is water. The solution is prone to crystallization at high concentration. Some metals are also prohibitively expensive and corrosive. For improving heat mass transport capacities, some additives are added to LiBr/water as a corrosion inhibitor. Therefore, an ammonia/water (NH₃/H₂O) absorption system is most commonly used where a lower temperature is required. The high concentration (rich solution) of ammonia (0.56 or 56%) is used in the present system comparing to conventional system (0.38) to increase the performance of the combined system/cycle.

Although LiBr/water and NH₃/water are used extensively for several years, essential studies on novel fluids have been done. For example, refrigerants were used to study fluorocarbon working fluids. Furthermore, because of its high solubility in many organic solvents, researchers suggested R22 and R21 widely. In addition, Dimethylformamide (DMF) and dimethyl ether of Tetra Ethylene Glycol (DMETEG) are used as emerging solvents.

3.3 Hot run simulation

The same operation of cold running is repeated with steam circulated to the generator and the Axial fan should be ON this will cool down the Absorber and condenser. Here again, soft water is used for cleaning the system with a level maintained.

After doing all operations till steam supply is started. The steam valve is to be slowly opened to give circulating water temperature as 110°C maximum. Continue circulation of chilled water for 2 hours. Stop steam and stop circulation pump. Drain all dirty water from the lowest drain point. Clean pump suction filter. Vent condenser to atmospheric condition.

3.4 Initial filling

Water: The following equipment is to be filled with mixture of Dimethylformamide (DMF) solvent water for chemical reactions.

- Rich tank, Solution exchanger and Shell and tube side.
- Generator Bottom, Pumps and pipeline.
- Do filling of water.
- Start pump on re-circulation.
- Keep Axial Fan ON Always.
- Fill chiller with NH₃. Keep the Absorber vent open in a bucket of water and check that NH₃ is not escaping. After rich tank pressure rises, take to liquor to the generator. Steam will pressurize the generator, and return ammonia to the condenser.
- Vent air from the condenser is dipped in a bucket of water and check that NH₃ is not escaping.
- Isolate NH₃ filling line after NH₃ tank level is reached. All NH₃ vapour is recovered by Lean solution in Absorber.

3.5 HP side stabilization

- NH₃ condenses at 45°C when pressure is 17 bars. To reach this pressure generator steam addition and condenser Axial Fan Running is necessary.
- Check the rich pump is running and open the letdown valve.
- Ensure that level is not lost in the rich tank and lean level.

- Open steam valve slowly, checking the rise in pressure.
- Close condenser vent after checking all air is purged out of the system.

3.6 Total stabilization

- Stabilize pump circulation between low pressure (LP) and high pressure (HP) side after closing by-pass to the chiller. Vent all high points to purge the air block.
- Start chilled water circulation slowly and increase Absorber pressure.
- Circulate steam into generator slowly to bring the temperature to design
- Check Rich pump temperature remains at below 55°C.

3.7 Normal operation

- When Chiller-Absorber pressure is going more than design, steam quantity is to be increased, to make it normal.
- When condenser pressure is going more than 19 atm, check axial Fan is running. Reduce the steam flow to reduce the pressure.
- When chiller pressure is lowering chilled water flow is to be increased to extract colder or if a load is not needed, reduce steam.
- Check the level in, rich tank, Lean tank, NH₃ tank.
- Check chiller and generator temperature conditions are normal.

Table 1 shows the pressure and temperature values taken during the experiments in different components of a GAX-VAS system.

The system performance is more efficient because NH₃ has a high latent heat of vaporization. The normal freezing point of NH₃ is -78°C, so it can be used for low-temperature cooling applications. The rectifier is used in a cycle to strip away water that normally evaporates with NH₃, since both NH₃ and water are volatile. The water would accumulate in the evaporator and offset the system performance if rectifier is not used. The disadvantages of NH₃/water are toxicity, high pressure and corrosive action with copper and copper alloy used in the system. However, NH₃/water is available at low cost environmentally friendly.

Table 1. Experimental data on VAS-GAX

Time (pm)	P ₁	P ₂	P ₃	P ₄	T ₁	T ₂	T ₃	T ₄	T ₅	T ₆
2.30	16	2	0.25	4.1	47	130	50	40	32	32
2.40	15.5	2	0.25	4.2	47	129	50	40	32	32
2.50	16.5	1.75	0.175	4.6	48	129	50	40	32	29
3.00	17	1.8	0.175	4.9	47	130	52	41	32	28.7
3.10	17	1.6	0.15	4.6	46	129	52	41	30.5	27.5
3.20	18.5	1.9	0.175	3.9	46	130	52	41	31	27
3.30	17.5	1.5	0.2	4	47	129	52	40	31	27
3.40	17	1.75	0.175	4.5	45	130	50	40	31	26.9
3.50	17.5	2	0.2	4.4	47	128	50	40	30.5	25.6
4.00	17	1.75	0.2	4	45	128	50	40	27.7	26
4.10	18	1.8	25	4.9	46	124	50	40	27.2	25.4
4.20	18	2	0.2	4.2	46	125	52	41	25.9	24.6
4.30	16	1.5	0.15	P4	45	124	52	40	25.3	24.6
4.40	16.5	1.6	0.15	4.1	47	124	52	40	25.5	24.6
4.50	17	2	0.15	4.2	46	126	52	40	25.4	24.7
5.00	16.5	1.8	0.15	4.6	46	128	52	40	25.9	25.2

Note: P₁- HP, P₂-LP, P₃-Water Pressure, P₄- Steam Pressure, T₁-Pump outlet, T₂-Lean outlet, T₃-Generator Inlet, T₄ – Condenser inlet, T₅- Chiller Inlet, T₆-Chiller outlet.

Table 2. Inlet and outlet temperature of major components in a system

Water	Generator	Condenser	Absorber	Evaporator
Inlet Temperature	100°C	20°C	20°C	20°C
Outlet Temperature	90°C	24°C	24°C	12°C

Table 3. Governing equations for major components of GAX-VAS system

Generator	Condenser	Evaporator	Absorber
$Q_g + Q_3 = Q_4 + Q_7$ $Q_3 = m_3 \cdot h_3$ $Q_4 = m_4 \cdot h_4$ $Q_7 = m_7 \cdot h_7$	$Q_c + Q_8 = Q_7$ $Q_8 = m_8 \cdot h_8$ $Q_7 = m_7 \cdot h_7$	$Q_e + Q_9 = Q_{10}$ $Q_9 = m_9 \cdot h_9$ $Q_{10} = m_{10} \cdot h_{10}$	$Q_a + Q_1 = Q_6 + Q_{10}$ $Q_1 = m_1 \cdot h_1$ $Q_6 = m_6 \cdot h_6$ $Q_{10} = m_{10} \cdot h_{10}$
$m_3 \cdot X_3 = m_4 \cdot X_4$ $m_1 = \frac{m_4 \cdot x_s}{x_w}$ $m_6 = \frac{m_{10}}{(1 - x_6/x_1)}$			$T_5 = -\epsilon - \frac{T_4}{(T_4 - T_2)} x(T_4 - T_2)$
$h(T, X) = 100 \sum_{i=1}^{16} a_i \left[\frac{T}{273.16} - 1 \right]^{m_i} (X)^{n_i}$ - Enthalpy at all thermodynamic state calculated with the help of Table 3			
$Q_g = (m_7 \cdot h_7) + (m_4 \cdot h_4) - (m_3 \cdot h_3)$ $Q_g = m_{11} \times 4.2 \times (T_{12} - T_{11})$	$Q_c = (m_7 \cdot h_7) - (m_8 \cdot h_8)$ $Q_c = m_{15} \times 4.2 \times (T_{16} - T_{15})$	$Q_e = (m_{10} \cdot h_{10}) - (m_9 \cdot h_9)$ $Q_e = m_{17} \times 4.2 \times (T_{18} - T_{17})$	$Q_a = (m_6 \cdot h_6) + (m_{10} \cdot h_{10}) - (m_1 \cdot h_1)$ $Q_a = m_{13} \times 4.2 \times (T_{14} - T_{13})$
$m_{11} = \frac{(m_7 \cdot h_7) + (m_4 \cdot h_4) - (m_3 \cdot h_3)}{42x(T_{11} - T_{12})}$	$m_{15} = \frac{(m_7 \cdot h_7) - (m_8 \cdot h_8)}{42x(T_{16} - T_{15})}$	$m_{17} = \frac{(m_{10} \cdot h_{10}) - (m_9 \cdot h_9)}{42x(T_{18} - T_{17})}$	$m_{13} = \frac{(m_6 \cdot h_6) + (m_{10} \cdot h_{10}) - (m_1 \cdot h_1)}{42x(T_{14} - T_{13})}$

Table 4. Coefficient of the enthalpy equation

SI No	m_i	n_i	a_i
1	0	1	-7.6108
2	0	4	25.6395
3	0	8	-247.092
4	0	9	325.952
5	0	12	-158.854
6	0	14	61.9084
7	1	0	14.1314
8	1	1	1.18157
9	2	1	2.84179
10	3	3	7.41609
11	5	3	891.844
12	5	4	-1613.09
13	5	5	622.106
14	6	2	-207.588
15	6	4	-6.87393
16	8	0	3.50716

The governing equations and the co-efficient used for the performance analysis for major components of GAX-VAS System are shown in Table 3 and 4. The system is divided into two sections with pressure limits, one for generator temperature (T_7) and another for evaporator temperature (T_{10}), with $P_1 = P_6 = P_9 = P_{10}$ corresponding to low pressure and $P_2 = P_3 = P_4 = P_5 = P_7 = P_8$ corresponding to high pressure.

3.8 Input data for the experiment

- Refrigerant mass flow rate = 0.05 kg/s
- Heat exchanger effectiveness = 0.7
- Temperature at Generator = $T_G = T_4 = T_7 = 50^\circ\text{C}$
- Temperature at Condenser = $T_C = T_8 = 50^\circ\text{C}$
- Temperature at Absorber = $T_A = T_1 = T_2 = 20^\circ\text{C}$
- Temperature at Evaporator = $T_E = T_{10} = T_9 = 2.5^\circ\text{C}$
- Weak solution concentration = $(X_w) = 55.3\%$
- Strong solution concentration = $(X_s) = 56\%$

4. SOLUBILITY DATA OF NH₃ IN WATER

4.1 Chiller

Figure 3 illustrates the liquid NH₃ vapour Pressure-Temperature relationship in chiller or evaporator. At 4 kg/cm², operating pressure, evaporator temperature is 4°C.

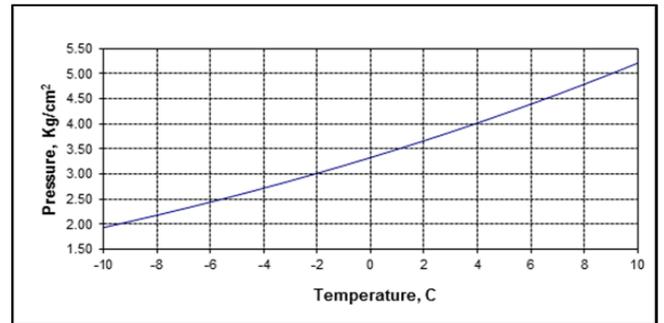


Figure 3. Variation of pressure with the temperature at Chiller

4.2 Condenser

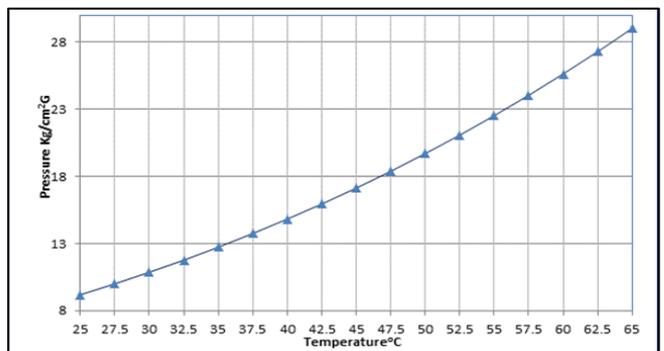


Figure 4. Variation of pressure with the temperature at Condenser

Figure 4 illustrates the liquid NH₃ vapour Pressure-Temperature relationship in condenser. For 50°C temperatures in condenser by running Axial Fan operating pressure is 19.7 kg/cm².

4.3 Absorber

Figure 5 illustrates the solubility data of NH₃ in water in absorber under pressure and particular temperature. At achieved absorber bottom temperature of 49°C with chiller operating at 4 kg/cm², 42% rich NH₃ concentration obtained from absorber.

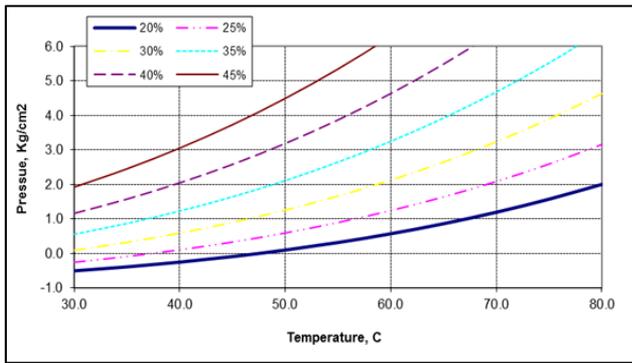


Figure 5. Variation of pressure with the temperature at Absorber

4.4 Generator

Figure 6 illustrates the solubility values of NH₃ in water in the generator under pressure and a particular temperature maintained by heating. At maintained bottom distiller temperature of 140°C and with condenser pressure of 17 kg/cm² achieved by running Axial Fan, 24% NH₃ concentration obtained from generator. Depletion of concentration is 18%.

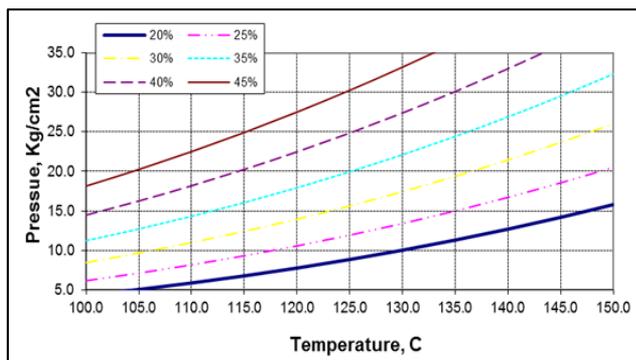


Figure 6. Variation of pressure with the temperature at Generator

5. RESULTS AND DISCUSSIONS

5.1 Thermodynamic analysis of VAS-GAX system

To conduct thermodynamic analysis of the proposed Vapour Absorption Cooling System (VACS), the following assumptions are made: There are no pressure variations other than those induced by the flow pump. At points 1, 4, and 8,

only Saturated Liquid exists, but Saturated Vapor exists at point 10. Pumping is an entirely isentropic operation. Assume that the weak solution is cooler and less absorbent, whereas the robust solution is more absorbent and cooler. The percentage of weak solutions in states 1–3 will stay unchanged, as will the percentage of strong solutions in states 4–6. “Temperatures at Thermodynamic States 11, 12, 13, 14, 15, 16, 17, and 18 represent the external water circuit used to give heat to the system’s components”, as shown in Figure 1. The inlet and outlet temperatures of the major components of the absorption system is illustrated in Table 2.

5.2 Performance (COP) analysis of VAS-GAX system

The working fluid’s chemical and thermodynamic properties are critical to the performance of absorption refrigeration systems. A critical condition for absorbent/refrigerant combinations is that they have a margin of miscibility in the liquid phase within the operational temperature range of the cycle. It must also be chemically stable, non-toxic, and non-explosive. In addition to these requirements, the following are desirable.

The difference in boiling point pressure between the pure refrigerant and the combination known as boiling elevation should be as significant as possible at the same pressure. The coolant must have a high heat of vaporization and a high concentration within the absorbent to maintain a low circulation rate between the generator and the absorbent per unit of cooling capacity. Heat and mass transfer are influenced by transport properties such as viscosity, thermal conductivity, and diffusion coefficient, which should all be favourable. Both the refrigerant and the absorbent should be non-corrosive, non-harmful to the environment, and affordable.

5.2.1 Generator

Figure 7 depicts the variation of COP with generator temperature. The results show that when the generator temperature rises, the Coefficient of Performance decreases due to corresponding enthalpy. This is because the generator load rises due to an increase in refrigerant enthalpy. The key advantage of this cooling system is that it can function at a low generator temperature to a low evaporator temperature while maintaining an appropriate COP system. Because fluid temperatures are generally low from this type of heat source, it can then use heat and solar industrial or civil wastes.

Figure 8 shows the heat input to the generator corresponding to the generator temperature. The result clearly shows that as the generator temperature increases the rate of heat supplied to generator decreases due to increase of absorber heat rejection rate.

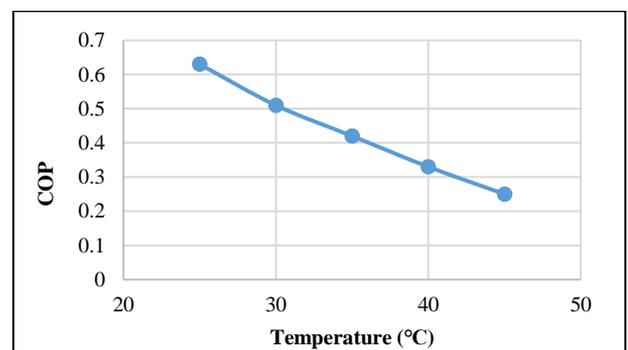


Figure 7. Variation of COP with generator temperature

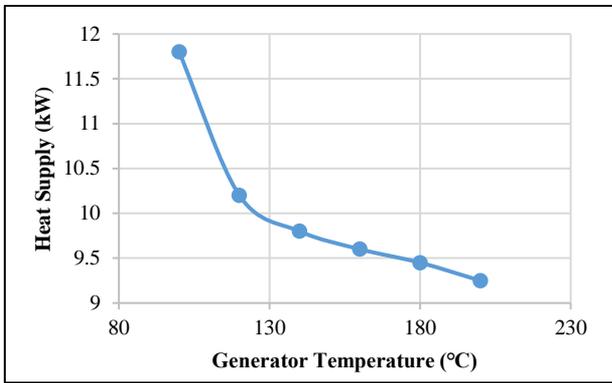


Figure 8. Variation of heat supply with generator temperature

5.2.2 Absorber

The link between COP and absorber temperature is depicted in Figure 9. The results show that when the temperature of the absorber decreases, so does the system's Coefficient of Performance. Because the generator load has dropped, this is the case.

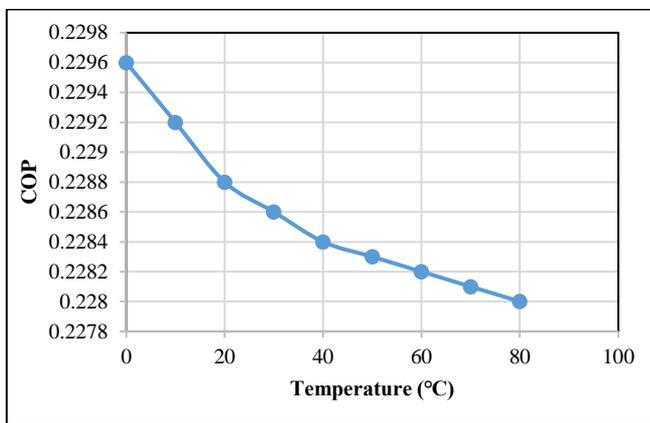


Figure 9. Variation of COP with absorber temperature

5.2.3 Evaporator

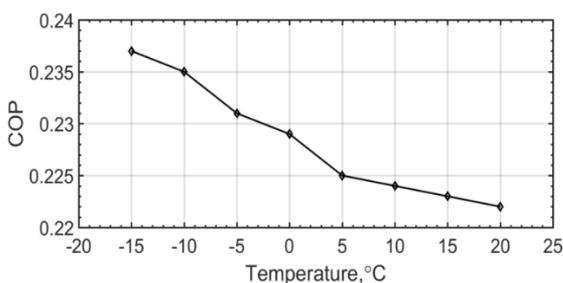


Figure 10. Variation of COP with evaporator temperature

The basic function of an evaporator in the refrigerator system is to remove the heat from the water, air, and other substances present in the refrigerator. The evaporators of refrigerator systems act as a heat exchanger which helps in transferring the heat from the substance and make it cool. The COP variation as a function of evaporator temperature is illustrated in Figure 10. As the evaporator temperature rises, the system's coefficient of performance appears to decrease with constant generator, condenser, and absorber temperatures. This is due to an increase in evaporator load. COP decreases

with the increase of thermal load; this is because of higher operating temperature and pressure of condenser. The literature study reveals that 75% load condition in the evaporator gave better results in terms of higher refrigeration effect and COP [15].

6. CONCLUSIONS

A modified VAS-GAX refrigeration system is fabricated with modern design and analyzed the experimental data to improve performance compared to the existing systems. The current system has a high COP when compared to existing VCS and VAS. The maximum COP obtained from the modified GAX system based on a greater generator temperature is 0.63 which is higher than that (0.1-0.3) of the standard absorption refrigeration system. In addition, the GAX cycle requires less electricity, since the system replaces the compressor. Also, the losses due to mechanical components are reduced. Further, the environmental damages were reduced due to the usage of non-toxic refrigerants. The modified VAS-GAX system is used for industrial applications due to high-performance values. Thus, the research on VAS-GAX system shall be extended by the researchers for more performance-based on commercial and industrial cooling applications.

ACKNOWLEDGMENT

The author declares and acknowledges receipt of funding from AICTE-RPS, Government of India, for a pilot project for Fabricating and experimentally analyze the performance of the GAX absorption system for cooling applications.

REFERENCES

- [1] Jain, V., Sachdeva, G., Kachhwaha, S.S. (2015). Energy, exergy, economic and environmental (4E) analyses based comparative performance study and optimization of vapor compression-absorption integrated refrigeration system. *Energy*, 91: 816-832. <https://doi.org/10.1016/j.energy.2015.08.041>
- [2] Dubey, A.M. (2020). Modified vapour absorption refrigeration cycles. *International Journal of Ambient Energy*, 74: 1-7. <https://doi.org/10.1080/01430750.2020.1720807>
- [3] Srivastava, S., Sen, R.K., Thakur, A., Tated, M.K. (2015). Review paper on analysis of vapour absorption refrigeration system. *International Journal of Research in Engineering and Technology*, 4(6): 410-413.
- [4] Boudéhenn, F., Bonnot, S., Demasles, H., Lefrançois, F., Perier-Muzet, M., Triché, D. (2016). Development and performances overview of ammonia-water absorption chillers with cooling capacities from 5 to 100 kW. *Energy Procedia*, 91: 707-716. <https://doi.org/10.1016/j.egypro.2016.06.234>
- [5] Osta-Omar, S.M., Micallef, C. (2017). Effect of the vapour-solution interface area on a miniature lithium-bromide/water absorption refrigeration system equipped with an adiabatic absorber. *Energy Procedia*, 118: 243-247. <https://doi.org/10.1016/j.egypro.2017.07.009>
- [6] Ramesh, R., Murugesan, S.N., Narendran, C., Saravanan, R. (2017). Experimental investigations on shell and

- helical coil solution heat exchanger in NH₃-H₂O vapour absorption refrigeration system (VAR). *International Communications in Heat and Mass Transfer*, 87: 6-13. <https://doi.org/10.1016/j.icheatmasstransfer.2017.06.010>
- [7] Jain, V., Sachdeva, G., Kachhwaha, S.S. (2018). Comparative performance study and advanced exergy analysis of novel vapor compression-absorption integrated refrigeration system. *Energy Conversion and Management*, 172: 81-97. <https://doi.org/10.1016/j.enconman.2018.06.116>
- [8] Al-Amir, Q.R., Khudair, N.Y. (2018). Theoretical analysis on the performance of branched GAX chiller cycle. *The Iraqi Journal for Mechanical and Material Engineering*, 18(4): 550-563.
- [9] Ponshanmugakumar, A., Rajavel, R. (2019). Experimental analysis of vapour absorption generator integrated with thermal energy storage system. *Materials Today: Proceedings*, 16(2): 1158-1167. <https://doi.org/10.1016/j.matpr.2019.05.209>
- [10] Talpada, J.S., Ramana, P.V. (2019). A review on performance improvement of an absorption refrigeration system by modification of basic cycle. *International Journal of Ambient Energy*, 40(6): 661-673. <https://doi.org/10.1080/01430750.2017.1423379>
- [11] Praveen, P., Santhosh, S., Raaghul, R., Kumar, A.S.P. (2020). Performance analysis of vapour absorption refrigeration system using waste heat from IC engine. *International Journal of Advanced Science and Technology*, 29(5): 10879-10892.
- [12] Lima, A.A., Leite, G.D.N., Ochoa, A.A., dos Santos, C.A., da Costa, J.A., Michima, P.S., Caldas, A. (2021). Absorption refrigeration systems based on ammonia as refrigerant using different absorbents: Review and applications. *Energies*, 14(1): 48. <https://doi.org/10.3390/en14010048>
- [13] Jain, V., Singhal, A., Sachdeva, G., Kachhwaha, S.S. (2020). Advanced exergy analysis and risk estimation of novel NH₃-H₂O and H₂O-LiBr integrated vapor absorption refrigeration system. *Energy Conversion and Management*, 224: 113348. <https://doi.org/10.1016/j.enconman.2020.113348>
- [14] Tetemke, Y., Paramasivam, V., Tadele, F., Selvaraj, S.K. (2021). Analyzed of vapor absorption refrigeration systems powered by geothermal energy: Site in Ethiopia. *Materials Today: Proceedings*, 46(17): 7570-7580. <https://doi.org/10.1016/j.matpr.2021.01.642>
- [15] Sriksirin, P., Aphornratana, S., Chungpaibulpatana, S. (2001). A review of absorption refrigeration technologies. *Renewable and Sustainable Energy Reviews*, 5(4): 343-372. [https://doi.org/10.1016/S1364-0321\(01\)00003-X](https://doi.org/10.1016/S1364-0321(01)00003-X)

NOMENCLATURE

B	dimensionless heat source length
C_p	specific heat, J. kg ⁻¹ . K ⁻¹
h	enthalpy Kj/kg
k	thermal conductivity, W.m ⁻¹ . K ⁻¹
m	Mass, kg
m_i, n_i, a_i	Co-efficient
Nu	local Nusselt number along the heat source
P	Pressure, Nm ⁻²
Q	Heat transfer at different components, kJ
T	Temperature, K
X	Concentration

Greek symbols

α	thermal diffusivity, m ² . s ⁻¹
β	thermal expansion coefficient, K ⁻¹
ϕ	solid volume fraction
θ	dimensionless temperature
μ	dynamic viscosity, kg. m ⁻¹ .s ⁻¹
Σ	sum

Subscripts

a	absorber
c	condenser
e	evaporator
g	generator
p	nanoparticle
f	fluid (pure water)
i	terms
nf	Nanofluid
$1,2,3,\dots$	state