P and S wave velocity of rocks in Jharia coalfield region for assessment of its geotechnical properties in dry, semisaturated and saturated conditions

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ABSTRACT. P-wave and S-wave velocity of the rock samples (Shale, Sandstone, Coal and Shaley sandstone) were determined in the laboratory in dry, saturated and partially saturated condition to determine the geotechnical rock properties of rock samples. The aim of this study was to predict the rock properties such as uniaxial compressive strength, tensile strength, and S wave from P-wave in dry, Semi saturated and Saturated condition. Highest values of P-wave velocities were obtained in a saturated condition and lowest values were obtained in dry condition. Different geotechnical properties of rock were determined in the laboratory. Utilizing the generated data, sets of empirical equations were developed between P-wave and relevant quantified rock parameters. The validity of the obtained empirical equations was confirmed using statistical analysis. Linear equations have been developed in this paper for estimation S-wave velocity, Uniaxial compressive strength (UCS) and tensile strength in both dry, partially saturated and semi-saturated rock conditions.

RÉSUMÉ. La vitesse des vagues P et S des échantillons de roche (schiste, grès, charbon et grès de Shaley) a été déterminée en laboratoire dans des conditions sèches, saturées et partiellement saturées afin de déterminer les propriétés géotechniques des échantillons de roche. Le but de cette étude était de prédire les propriétés de la roche telles que la résistance à la compression uniaxiale, la résistance à la traction et les vagues P et S dans des conditions sèches, semi-saturées et saturées. Les valeurs les plus élevées de la vitesse de la vague P ont été obtenues à l'état saturé et les valeurs les plus basses ont été à l'état sec. Différentes propriétés géotechniques de la roche ont été déterminées en laboratoire. À l'aide des données générées, des ensembles d'équations empiriques ont été développés entre les paramètres de la vague P et de la roche quantifiés pertinents. La validité des équations empiriques obtenues a été confirmée par analyse statistique. Des équations linéaires ont été développés dans cet article pour l'estimation de la vitesse de la vague S, de la résistance à la compression uniaxiale (UCS en anglais) et de la résistance à la traction des roches sous les conditions sèche, partiellement saturée et semi-saturée.

KEYWORDS: P-wave velocity, S-wave velocity, rock properties, coal mines, rock samples.

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MOTS-CLÉS: vitesse de la vague P, vitesse de la vague S, propriétés des roches, mines de charbon, échantillons de roche.

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1. Introduction

P-wave and S-wave velocities can be determined both in the laboratory as well as the field. It is the most common non-destructive test method used in civil, geotechnical and mining projects such as underground opening, quarrying, blasting and ripping. Seismic waves can also be used to predict the rock mass deformation, stresses developed around the opening in underground or opencast mines or tunnels and also in blasting. (Onodera, 1963; Hudson et al., 1980; Gladwin, 1982). Thill and Bur (1969) found that the P-wave velocity changes with porosity and degree of saturation. A rise in the P-wave velocity. Several researchers (Hawkins and McConnell, 1992; Ulusay et al., 1994; Tuğrul and Zarif, 1999; Kahraman, 2001; Yasar and Erdogan, 2004; Kahraman and Yeken, 2008; Sharma and Singh, 2008; Yagiz, 2009) reported that the P wave has a relationship with some rock properties such as uniaxial compressive strength, hardness, density and slake durability index of rock as shown in table 1. However, obtained correlations are not constant and can be varied with rock types. The p-wave velocity of wet rock can be predicted from the P-wave velocity of dry rock (Kahraman, 2007). This paper attempts to investigate the empirical relationship between P-wave and S-wave and rock properties including the uniaxial compressive strength (UCS), Modulus of elasticity (E), Porosity, water absorption by weight (w), and both saturated (ρ_{sat}) and dry (ρ) density of rocks.

Researchers name	Equations	R – value	Rock type	UCS (M Pa)	Vp(Km /s)
Tugrul and Zarif 1999 [7]	UCS=35.54Vp-55	0.8	Igneous rock	100-200	4.5-6.5
Kahraman 2001[8]	UCS=9.95Vp ^{1.21}	0.83	Limestone, Ma rble	10-160	1.2-6.4
Yasar and Erdogan 2004	UCS=(Vp-2.0195) /0.032	0.81	Lime, marble,	38-120	2.9-5.6
[9]	ρ=(Vp+7.707)/4.3 183	0.80	dolomite	2.43-2.97	2.9-5.6
Kahraman And Yeken 2 008 [10]	ρ=0.213Vp+1.256	0.82	Carbonate roc ks	2.0-2.6	3.6-6.1
Sharma And Singh 2008 [11]	UCS=0.0642Vp-1 17.99	0.90	7 types pf rock s	10-1970	2-3
Vacia 2000 [12]	UCS=0.258Vp ^{3.543}	0.92	0 trunce of reals	20-125	1.89-6. 1
1 agiz 2009 [12]	UCS=49.4Vp-167	0.89	9 types of rock		-
	ρ=0.19Vp+1.61	0.69		2.15-2.85	1.8-6.1

Table 1. Relationship between Vp. p a	and UCS
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The classification of p wave velocity of rocks is shown in Table 2 was done by Anon in 1979.

Minear (1982) showed that clay suspended in the pores of sandstone has only a small effect on velocities, whereas both structure and laminated clay result in a dramatic velocity reduction. The presence of pore space reduces the bulk density of the rock. This would appear to increase P-wave and S-wave velocity due to the reduction in density. The effect of a general decrease in P-wave and S-wave velocity with increasing porosity is due to the increase in porosity reducing the rigidity of the rock that decreases both P-wave and S-wave. Pore structure has an effect on both bulk and shear modulus. The p-wave velocity of wet rock can be predicted from the P-wave velocity of dry rock.

Serial no.	Vp (in km/s)	Description		
1	Less than 2.5	Very low		
2	2.5 - 3.5	Low		
3	3.5 - 4.0	Moderate		
4	4.0 - 5.0	High		
5	Greater than 5	Very High		

Table 2. Classification of rocks on the basis of p wave velocities

2. Field work and laboratory work

Rock samples were collected from different mines located in the Jharia coalfield region prior to blasting from the benches. The location of the mines is shown in figure 1. Generally, in coal mines, three types of materials encountered in the overburden are Sandstone, shale and shaly sandstone. So, different rock type was collected from each mine. Samples consisted of coal, sandstone, shale and shaley sandstone. Shaley sandstone is the most common occurring rock type in the Indian coal mines in the form of overburden. Each rock block was inspected to ensure that it would provide standard testing specimens without macroscopic defects, alteration zones and fractures. Samples were prepared following the ISRM standards 1981 (Brown, 1981). Relevant rock properties such as Vp, Vs, UCS, Tensile strength and bulk density. For each rock test, 5 different rock samples were taken. Entire rock mass was carried on intact rock mass.

Dry sample preparation: The samples were oven dried at $110 \circ C$ as shown in figure 2 and there P and S wave velocity was determined. The weight of the samples was taken on weighing machine having least count 0.1 kg as shown in figure 3. Semi saturated sample preparation: Than the samples were kept for one hour immersed in water for partial saturation and its P and S wave velocity was determined. Completely Saturated Sample: Sample was kept for 72 hours immersed in water to attain its full saturation as shown in figure 4. The weight of the samples was measured using a weighing machine of 0.1g least count as shown in figure 4. P wave and S wave velocity of the collected rock samples were determined using

Sonic viewer as shown in figure 5 and 6 respectively. The determination was done in dry, and completely saturated condition.



Figure 1. Sample collecting location of different coal mines in Jharia coalfield area



Figure 2. Samples in oven for drying



Figure 3. Samples being weighed



Figure 4. Samples immersed in water

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Figure 5. P wave velocity of rock



2.1. Materials used in the study

2.1.1. Coal

Serial	Density(g/cc)	P wave	S wave	UCS	Tensile strength
no.		(km/s)	(km/s)	(Mpa)	(Mpa)
1	1.45	2.92	0.68	12.01	1.65
2	1.34	1.72	0.52	8.57	1.26
3	1.45	3.86	0.81	19.25	1.81
4	1.43	3.37	0.69	14.44	1.63
5	1.44	3.48	0.74	18.13	1.79
6	1.49	3.75	0.84	18.25	1.73
7	1.49	3.59	0.94	16.65	1.61
8	1.36	2.5	0.61	14.52	1.62
9	1.34	1.92	0.56	9.56	1.47
10	1.4	2.01	0.57	10.71	1.51

Table 3. Results of different tests conducted on samples

Table 4. Obtained relationships between p wave and rock properties

Sl no.	Material	Rock property	Regression equation	\mathbb{R}^2	Range	
1	Coking coal	Density	y=0.2672x ^{6.7269}	0.7859	1.34 -1.49 g/cc	
2	Coking coal	UCS	y=4.4299x+1.309	0.8778	8.57 -19.25 Mpa	
3	Coking coal	S wave	y=1.522x+0.529	0.8231	0.56 – 0.94 km/s	
4.	Coking coal	Tensile strength	0.1745x+1.0999	0.7566	1.26 – 1.81 MPa	

10 coal samples were tested for determination of P-wave, S-wave UCS and tensile strength. The bulk density of coal was determined by immersing the sample in the water. Tensile strength and shear strength of the coal sample was also determined in the laboratory. From figure 7 it is observed that S-wave velocity is directly proportional to P wave velocity. A plot of P wave velocity and density, S

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wave, uniaxial compressive strength, and tensile strength is shown in figure 7 respectively.

Figure 7. Plot between p wave velocity and tensile strength, density, UCS and Swave of coal

From Figure 7, it is evident that that as the density of the material increases the P-wave velocity also increases. The relations found are as follows in Table 4:

2.2.2. Sandstone

10 samples of sandstone were kept in the P and S-wave testing apparatus was determined and results are shown in table 5 for each of the three conditions. The coal samples were in dried condition saturated and semi-saturated. The semi-saturated samples were prepared by immersing the samples in water for 1 hour. The samples were cored from it blocks brought from different mines. The bulk density was determined by immersing the sample in the water and the tensile strength and shear strength was also determined. The S-wave was undetected for compressive samples due to its large length. Tensile strength and uniaxial compressive strength were determined in the laboratory.

From Figure 8, It is found that the relation between properties of sandstone such as S-wave, UCS and Tensile strength vs P-wave in all three conditions i.e. dry, semisaturated and saturated is different. The relations obtained in dry samples were found to be more suitable for prediction of geotechnical properties of rock due to its high correlation coefficient values. Hence, it is recommended to use dry P-wave velocity for predictions. The relations found are as follows Table 6.

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Seri al n o	Dr y de ns ity (g /c c)	P w av edr y (k m/ s)	S w av edr y (k m/ s)	Semi- S aturated density (g/cc)	P w aves emi sa turate d (km /s)	S w aves emi sa turate d (km /s)	Satura ted de nsity (g/cc)	P wa ves atura ted (k m/ s)	S wa ves atura ted (k m/ s)	Uniaxial c ompressiv e strength (Mpa)	Tensil e stren gth (Mpa)
1	2. 54	3. 23	0. 56	2.59	3.29	0.63	2.61	3.4 6	0.7 5	39.98	7.48
2	2. 54	3. 12	0. 68	2.58	3.24	0.64	2.6	3.5 1	0.5 3	33.07	7.27
3	2. 54	3. 32	0. 57	2.55	3.35	0.8	2.61	3.4 2	0.5 2	39.47	7.97
4	2. 58	3. 53	0. 51	2.59	3.55	0.62	2.62	3.7 1	0.5 1	47.24	8.95
5	2. 58	3. 39	0. 54	2.59	3.45	0.74	2.61	3.6 3	0.5 2	38.97	7.54
6	2. 55	3. 23	0. 64	2.58	3.29	0.51	2.6	3.5 8	0.6 1	38.24	7.33
7	2. 52	3. 01	0. 67	2.55	3.09	0.54	2.57	3.5 2	0.5 7	32.47	7.11
8	2. 58	3. 53	0. 52	2.60	3.63	0.71	2.61	3.7 1	0.5 3	45.28	9.1
9	2. 57	3. 41	0. 55	2.58	3.43	0.56	2.61	3.5 1	0.5 4	42.34	8.54
10	2. 54	3. 2	0. 61	2.57	3.36	0.52	2.58	3.5 3	0.5 5	33.57	7.33
11	2. 55	3. 39	0. 49	2.57	3.45	0.74	2.59	3.5 5	0.6 1	41.24	7.52

Table 5. Results of sample





Figure 8. Plot between p wave velocity and tensile strength, desnity, UCS and Swave of sandstone

Sl	Material	Property	Condition of	Regression	R ²	Range
no.			material	equation		
1	Sandstone	Density	Dry	y = 7.1645x -	0.8074	2.52 - 2.58
				14.99		g/cc
			Semi	y = 1.8452x -	0.0892	2.55 - 2.6
				1.242		g/cc
			Saturated	y = 5.9063x -	0.4065	2.57 - 2.62
				11.847		g/cc
2	Sandstone	S-wave	Dry	y = 5.9986x-	0.7881	0.49 - 0.68
				1.966		km/s
			Semi	y=0.0979x ^{1.5319}	0.1925	0.51 - 0.8
						km/s
			Saturated	y=4.6474x ^{-1.663}	0.1485	0.51 - 0.75
						km/s
3	Sandstone	UCS	Dry	y=2.4896x ^{2.3033}	0.8869	32.47 -
			Semi	y=2.8666x ^{2.3332}	0.7069	47.24 Mpa
			Saturated	y=1.6268x ^{2.5039}	0.2794	
4	Sandstone	Tensile	Dry	y=1.3129x ^{1.4921}	0.7274	7.11 – 9.1
		strength	Semi	y=1.1115x ^{1.6301}	0.6657	Mpa
			Saturated	y=0.7312x ^{1.8661}	0.3096	

Table 6. Regression equation obtained from the plot

2.2.3. Shaly sandstone

Shaly sandstone rock is the combination of sandstone and shale. The shale band appears in layer between the sandstone. The p wave velocity was dependent on the thickness of the shale. The UCS and tensile strength were also affected by the shale band.

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S1	Dry	Р	S	Semi-	Ρw	S w	Satur	Р	S	Tensi	Uniaxia
n	den	wa	wa	Satur	aves	aves	ated	wa	wa	le stre	l compr
0.	sity	ve _d	ve _d	ated d	emi sa	emi sa	densi	ve _{sa}	ve _{sa}	ngth	essive s
	(g/c	ry	ry	ensity	turate	turate	ty (g/	turate	turate	(Mp	trength
	c)	(k	(k	(g/c	d	d	cc)	d	d	a)	(Mpa)
		m/	m/	c)	(km	(km		(k	(k		
		s)	s)		/s)	/s)		m/	m/		
								s)	s)		
1			0.4		1.7	0.5		1.1	0.5		
	2.55	1.8	7	2.58	1	6	2.6	2	6	5.72	18.34
2		3.1	0.6			0.6		1.4	0.5		
	2.6	3	9	2.61	2	4	2.63	4	7	8.11	36.23
3		2.1	0.5		2.1	0.6		1.0	0.5		
	2.61	5	7	2.63	5	5	2.66	3	8	6.99	27.97
4		2.8	0.6		2.7			1.3	0.6		
	2.62	4	2	2.63	5	0.7	2.64	1	3	7.59	36.82
5		2.6	0.6		2.6	1.0		1.8	1.2		
	2.61	5	8	2.62	5	3	2.65	4	4	7.25	31.46
6		2.3	0.6		2.1	0.6		1.2	0.6		
	2.57	6	3	2.6	7	4	2.62	3	6	7.10	33.25
7		2.5	0.6		1.8	0.4		1.3	0.5		
	2.61	7	3	2.64	7	9	2.66	4	6	7.25	30.97
8		1.9	0.4		1.6	0.4		1.4	0.6		
	2.57	9	9	2.58	7	7	2.61	1	3	5.60	21.08
9		2.2	0.5		1.9	0.4		1.5	0.5		
	2.59	5	6	2.61	8	9	2.63	1	4	6.25	31.24
1			0.5		1.6	0.5		1.1	0.5		
0	2.56	2.1	9	2.57	7	9	2.63	5	1	6.11	25.87

Table 7. Shaly sandstone sample results

From Figure 9, It is found that the relation between properties of shale sandstone such as S-wave, UCS and Tensile strength vs P-wave in all three conditions i.e. dry, semi-saturated and saturated is different. The relations obtained in dry samples were found to be more suitable for prediction of geotechnical properties of rock due to its high correlation coefficient values. Hence, it is recommended to use dry P-wave velocity for predictions. The relations found are as follows



Figure 9. Plot between p wave velocity and tensile strength, density, UCS and Swave of Shaly-sandstone

Sl no.	Material	Property	Condition of material	Regression equation	R ²	Range
			Dry	y= 11.794x - 28.618	0.5179	2.55 – 2.61 g/cc
1	Shaley- sandstone	Density	Semi	y=10.088x - 24.238	0.4026	2.57 – 2.64 g/cc
			Saturated	y=1.8726x + 3.5925	0.026	2.6 – 2.66 g/cc
	Shaley- sandstone		Dry	y=0.1558x + 0.2215	0.7721	0.47 – 0.69 (km/s)
2		S-wave	Semi	y=0.3242x - 0.0424	0.5849	0.47 – 1.03 (km/s)
			Saturated	y=0.6863x - 0.2702	0.5624	0.51 – 1.24 (km/s)
3	Shaley-	UCS	Dry	y = 13.195x + 2.1332	0.7954	18.34 -
	sanustone		Semi	v = 11.271x +	0.4473	50.62 Mpa

Table	8. I	Regression	equations	obtained	from a	plot o	f shaly	sandstone
		0	1				/ /	

				4.2911		
			Saturated	y=10.0995x + 12.82	0.1575	
			Dry	y=1.8832x + 2.3069	0.8624	
4	Shaley- sandstone	Tensile strength	Semi	y=1.4087x + 3.8917	0.4181	5.72 – 8.11 Mpa
		-	Saturated	0.8882x + 5.6079	0.0615	

2.2.4. Shale

Shale, any of a group of fine-grained, laminated sedimentary rocks consisting of silt- and clay-sized particles. Shale is the most abundant of the sedimentary rocks, accounting for roughly 70% of this rock type in the crust of the Earth. The p wave velocity, UCS, tensile strength and density was determined as shown in table 9. The relation between p wave and UCS, tensile strength, density, S-wave velocity is shown in figure 10.

Sl	Dry	Р	S	Semi-s	P wa	S wa	Satura	P w	S w	Tensil	UCS
n	densi	wa	wa	aturate	ve _{sem}	vesem	ted de	aves	aves	e stren	(Mp
о.	ty (g/	ved	ved	d densit	i satura	i satura	nsity	aturat	aturat	gth (M	a)
	cc)	ry	ry	y (g/cc)	ted	ted	(g/cc)	ed	ed	pa)	
		(k	(k		(km/	(km/	-	(km	(km		
		m/	m/		s)	s)		/s)	/s)		
		s)	s)								
1		4.1									
	2.34	7	0.5	2.36	3.66	0.56	2.4	1.66	0.5	7.31	16.6
2		4.4	0.5								30.9
	2.45	9	5	2.48	3.06	0.55	2.51	1.72	0.59	8.56	1
3		4.5	0.5								27.9
	2.46	4	9	2.49	3.02	0.57	2.53	1.56	0.53	9.27	3
4		4.1	0.5								17.2
	2.29	9	1	2.32	3.46	0.87	2.37	1.58	0.67	6.46	5
5		3.7	0.4								16.5
	2.19	9	9	2.24	3.74	0.79	2.31	1.85	0.63	5.79	7
6		4.1	0.5								20.3
	2.34	2	2	2.39	3.89	0.9	2.45	1.69	0.68	6.22	7
7		4.2	0.5								
	2.5	3	3	2.54	3.23	0.67	2.59	1.74	0.69	6.45	24.8
8		4.4	0.6								
	2.43	4	1	2.45	3.56	0.8	2.49	1.68	0.63	8.23	27.9
9		4.6	0.6								
	2.48	5	9	2.51	3.19	0.55	2.55	1.9	0.89	9.74	30.2
1		4.4	0.5								
0	2.5	3	9	2.52	3.09	0.52	2.58	1.77	0.63	7.56	28.4

Table 9. Test results of Shale



Figure 10. Plot between p wave velocity and tensile strength, density, UCS and Swave of shale

Serial	Material	Property	Condition of	Regression	Correlation	Range
no.			material	equation	coefficient	
1	Shale	Density	Dry	y=2.067x -	0.7142	2.19-2.5
				0.6516		g/cc
			Semi	y = -2.3804x +	0.565	2.24-2.54
				9.1744		g/cc
			Saturated	y=0.1308x +	0.013	2.31-2.59
				1.3909		g/cc
2	Shale	S-wave	Dry	y=0.2075x +	0.7169	0.5-0.69
				0.3352		km/s
			Semi	y=0.3509x -	0.5505	0.52-0.87
				0.5115		km/s
			Saturated	y=0.6334x -	0.4068	0.5-0.89
				0.4423		km/s
3	Shale	UCS	Dry	y = 20.156x +	0.7649	16.57-
				62.652		30.91 Mpa
			Semi	y = -14.402x +	0.594	
				72.941		
			Saturated	y=10.869x +	0.0397	
				5.4787		
4	Shale	Tensile	Dry	y=4.8933x -	0.8369	5.79-9.74
		strength		13.507		Мра
			Semi	y= -2.886x +	0.4429	
				17.343		
			Saturated	y = 0.4722x +	0.0014	
				6.7493		

Table 10. Regression equations obtained from plots of shale

From Figure 10, it is found that the relation between properties of shale such as S-wave, UCS and Tensile strength vs P-wave in all three conditions i.e. dry, semisaturated and saturated is different. The relations obtained in dry samples were found to be more suitable for prediction of geotechnical properties of rock due to its high correlation coefficient values. Hence, it is recommended to use dry P-wave velocity for predictions. The relations found are as follows Table 10.

3. Conclusions

From this study it is seen that in dry condition there is a strong correlation between the p wave value and other geotechnical parameters. This can be verified by the correlation coefficient values obtained for the dry sample condition was on the higher side. So the following conclusions can be drawn out from the study as shown in table 11.

Sl n o.	Material	Property	Condition of m aterial	Regression eq uation	R ²	Range
1	Coal	S-wave	Dry	y=4.4299x+1. 309	0.87 78	8.57-19.25 Mpa
		UCS		y=1.522x+0.5 29	0.82 31	0.56–0.94 k m/s
		Tensile str ength		0.1745x+1.09 99	0.75 66	1.26–1.81 Mpa
2	Sandstone	S-wave	Dry	y = 5.9986x-1. 966	0.78 81	0.49–0.68 k m/s
		UCS		$y=2.4896x^{2.303}$	0.88 69	32.47–47.24 Mpa
		Tensile str ength		$y=1.3129x^{1.492}$	0.72 74	7.11–9.1 M pa
3	Shaly-sand stone	S-wave	Dry	y=0.1558x + 0.2215	0.77 21	0.47–0.69 (k m/s)
		UCS		y = 13.195x + 2.1332	0.79 54	18.34-36.82 Mpa
		Tensile str ength		y=1.8832x + 2.3069	0.86 24	5.72–8.11 Mpa
4	Shale	S-wave	Dry	y=0.2075x + 0.3352	0.71 69	0.5–0.69 km /s
		UCS		y = 20.156x + 62.652	0.76 49	16.57–30.91 Mpa
		Tensile str ength		y=4.8933x - 1 3.507	0.83 69	5.79–9.74 Mpa

Table 11. The following observation can be drawn out from the study

This shall help field engineers (mining and civil) to estimate the geotechnical properties of rock without undergoing destructive tests. The samples can be preserved for a future test. This p wave test can be carried out on rock mass in the

field with the help of diode for better results. The laboratory results can also be normalized by the relation given by Barton for better estimation from laboratory P wave values. This shall be economical and time saving for industries in the assessment of rock properties for blasting and civil construction. As the testing process is tiresome and for every new test we require new samples as they are destructive tests. The samples also can be used in the future if preserved in a better way.

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