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The article presents the results of modeling the process of operation of seamless hot-

extruded pipes with helical inner ribbing of the inner surface. The modeling was carried out in the CAD software SolidWorks using the integrated calculation module Flow Simulation. After modeling and finding the coefficients of the linear regression function, the

corresponding equations were obtained for calculating the hydrodynamic and kinematic

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Simulation of Boiler Helical Inner Ribbing Surface Tubular Working

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parameters of the water-steam mixture flow.

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ABSTRACT

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1. INTRODUCTION

Finned pipes for heat exchangers are used in various fields: heating and air conditioning of residential premises and outbuildings, mechanical engineering, the oil industry, nuclear power [1-11].

Due to their special design, heat exchange tubes allow quick and efficient cooling of the coolant, thereby increasing the internal surface area and the heat transfer coefficient.

2. METHOD FLOW

Three-dimensional solid models of hot-extruded pipes with an outer diameter of 60.0 mm and a wall thickness of 6.0 mm were created in the amount of 49 pieces.

Sketches of cross-sections of ribs were placed at the same distance from each other when constructing helical ribbing of pipes.

Figure 1 shows, as an example, a solid model of a pipe with a ribbing of the inner surface, consisting of twelve ribs.

The angle of rise of the rib in the models varies from 0° (plain tube) to 45° in 15° increments. The higher the angle of rise, the more turns can fit along the length of the pipe. Figure 2 shows a longitudinal section of a pipe with a designation for the elevation angle to represent this parameter.

Computer simulation of the operation process of seamless hot-extruded pipes with helical ribbing of the inner surface in the CAD software SolidWorks using the integrated calculation module Flow Simulation [11-13] has been performed. Numerical values of the hydrodynamic and kinematic parameters of the process are obtained.

Geometry tools in the SolidWorks software make it easy to create ribbing on the inner surface of a pipe and to vary the angle of elevation of the rib by changing the step size.

The next step after creating three-dimensional solid models

of pipes with helical ribbing of the inner surface is to set the



Figure 1. Solid model of pipe with helical inner ribbing surface

Figure 2. Longitudinal section of the pipe with helical inner ribbing surface: α° – rib angle

Computer models of the operation process of seamless hotextruded pipes with helical ribbing of the inner surface were simulated in the SolidWorks software environment using the integrated calculation module Flow Simulation.





3. EXPERIMENTAL PART

The main parameters of the modeling process are shown in Table 1. For each of the 49 models, the same input parameters were set. Each pipe was modeled with two heat carriers watersteam mixture.

Table 1. Initial data for computer modeling

№	Parameter	Value	
1	Pipe material	Steel 20	
2	Pipe length	500 mm	
3	Surface roughness	60 mcm	
4	Ambient temperature	40 °C	
5	Initial pipe body temperature	20 °C	
6	Flow temperature	160 °C	
7	Flow pressure	0,156 MPa	
8	Flow time	60 c	
9	Heat carrier	water-steam mixture	

The output parameters of the computer simulation were the hydrodynamic and kinematic characteristics of the coolant flow, as well as the indicators of the change in the temperature of the solid. The output from the modeling process is presented in Table 2.

Table 2. Output data of the modeling process

N⁰	Parameter	Symbol	Dimension
1	Heat transfer coefficient	α2	$W/m^2 \cdot K$
2	Solid temperature (max.)	T_s	°C
3	Heat dissipation power	N _{ht}	W
4	Specific heat flux	η_{hf}	W/m^2
5	Friction force	$F_{\rm Tp}$	Ν
6	Turbulence energy	E_T	J/kg
7	Specific dissipation of the energy of pulsating motion under the action of viscosity	$ ho_arepsilon$	W/kg



(b) Seven-way ribbing

Figure 3. The nature of the movement of the coolant inside the pipe

The nature of the movement of the coolant inside the pipe is shown in Figure 3. As you can see, the flow is turbulent in nature, which is associated with the peculiarity of the geometry of the pipe, which ensures swirling and creation of vortex motion. With an increase in the number of calls, the flow rate increases, which is shown by the example of pipes shown in Figure 3 (a, b).

When carrying out computer modeling in the SolidWorks CAD software environment using the integrated calculation module Flow Simulation, the numerical values of the output data presented in Table 2 were obtained.

4. RESULT PROCESSING

The key parameters influencing the change in the hydrodynamic and kinematic characteristics of the coolant flow are the number of helical finning entries and the rib elevation angle, varying from 0 to 45 $^{\circ}$ due to an increase or decrease in the step between the turns of the generatrix, which constitutes the trajectory of motion when constructing the rib geometry.

To determine the equations for calculating the parameters of the process of modeling the operation of seamless hotextruded pipes with helical ribbing of the inner surface, depending on the change in the angle of the rib lift and their number, a regression analysis was carried out.

Due to the sufficient amount of data obtained in the course of computer modeling in the SolidWorks CAD software environment using the integrated calculation module Flow Simulation, it was possible to carry out regression analysis.

An experimental method was used to select the type of regression function.

Based on the principle of minimum complexity to analyze the dependence of each of the output parameters (Table 3) on the number of ribs and their elevation angle, a linear form of the regression function was adopted $-y = b_0 + b_1x + \dots + b_nx_n$. The parameters of this function were estimated by the least squares method (OLS) in Microsoft Office Excel.

After finding the coefficients of the linear regression function, the corresponding equations were obtained of the water-steam mixture flow:

$$\alpha_2 = 830,30 - 19,82 \cdot K_p + 6,65 \cdot \alpha^{\circ}, \tag{1}$$

where, α_2 – heat transfer coefficient, W/m² K; K_p – number of ribs; α° – rib angle;

$$N_{ht} = -6627,13 + 284,99 \cdot K_{\rm p} - 107,62 \cdot \alpha^{\circ}, \tag{2}$$

where, N_{ht} – heat transfer power, W;

$$\eta_{hf} = -122903,309 + 6008,807 \cdot K_{p} - 44,258 \cdot \alpha^{\circ}, \qquad (3)$$

where η_{hf} – specific heat flux, W/m²;

$$F_{\rm Tp} = 13,739 + 0,015 \cdot K_{\rm p} + 0,21 \cdot \alpha^{\circ}, \tag{4}$$

where, $F_{\rm Tp}$ – friction force, N;

$$E_T = 0.678 - 0.039 \cdot K_p - 0.003 \cdot \alpha^{\circ}, \tag{5}$$

where, E_T – turbulence energy, J/kg;

$$\rho_{\varepsilon} = 258,93 - 17,10 \cdot K_{\rm p} - 1,25 \cdot \alpha^{\circ}, \tag{6}$$

where, ρ_{ε} – specific energy dissipation, W/kg;

$$T_s = 159,87 + 0,004 \cdot K_p + 0,001 \cdot \alpha^{\circ}, \tag{7}$$

where, T_s – maximum temperature of a solid.

The number of fins should increase heat transfer. Therefore, it is planned to correct it in the future and work in this direction.

Comparison of the values calculated by formulas (1) - (7) with the values obtained in the simulation shows that these values have discrepancies within 28% for the parameters indicated in Table 1. This means that the selected regression function is adequate.

After finding the coefficients of the linear regression function, the corresponding equations were obtained similarly to Eqns. (1)–(7) for steam flow:

$$\alpha_2 = 2604,332 - 139,192 \cdot K_p - 3,024 \cdot \alpha^{\circ}, \tag{8}$$

$$N_{ht} = -205,247 - 3,809 \cdot K_{\rm p} - 10,756 \cdot \alpha^{\circ}, \qquad (9)$$

$$\eta_{hf} = -4667,01 + 35,613 \cdot K_{\rm p} - 62,842 \cdot \alpha^{\circ}, \qquad (10)$$

$$F_{\rm rp} = 0,008 - 0,0002 \cdot K_{\rm p} + 0,0002 \cdot \alpha^{\circ},$$
 (11)

$$E_T = 0.259 + 0.003 \cdot K_p + 0.0009 \cdot \alpha^{\circ}, \qquad (12)$$

$$\rho_{\varepsilon} = 97,592 - 0,07 \cdot K_{\rm p} + 0,144 \cdot \alpha^{\circ}, \tag{13}$$

$$T_s = 89,090 + 2,018 \cdot K_p + 1,167 \cdot \alpha^{\circ}.$$
 (14)

Comparison of the values calculated by formulas (8) - (14) with the values obtained by modeling in the Solid Works software shows that these values have discrepancies within 25%. This means that the selected regression function is adequate.

5. CONCLUSION

Computer simulation has been performed computer simulation of the operation process of seamless hot-extruded pipes with helical ribbing of the inner surface in the CAD software SolidWorks using the integrated calculation module Flow Simulation. Numerical values of the hydrodynamic and kinematic parameters of the process are obtained. Equations were obtained based on the data obtained and the performed regression analysis.

The results obtained in the course of the work can be useful for assessing the possible boundaries of intensification of heat transfer and assessing the applicability of pipes for the transfer of various heat carriers.

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