

Thermal radiation impact on boundary layer dissipative flow of magneto-nanofluid over an exponentially stretching sheet

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ABSTRACT

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The impact of thermal radiation on viscous dissipative boundary layer flow of heat absorbing magneto-nanofluid over a permeable exponentially stretching sheet with Navier's velocity and thermal slips has been analyzed. The prevailing mathematical equations are changed to nonlinear ordinary differential equations using the appropriate similarity variables and then the equations are numerically solved by Runge-Kutta scheme of fourth order together with the shooting technique. Three kinds of water based nanofluids having aluminum oxide, copper and titanium oxide as nanoparticles are considered for this investigation. The consequence of relevant flow parameters on nanofluid velocity, temperature distribution, wall velocity gradient and local Nusselt number are displayed by means of various graphs. In addition, analysis of quadratic regression estimation on the numerical data of coefficient of skin friction and local Nusselt number has been presented to verify the relationship among the controlling physical parameters and transfer rate parameters. Our result reveals that the velocity and temperature distribution profiles are lower for Cu-water nanofluid followed by Al₂O₃ and TiO₂ water base nanofluids in the regime of boundary layer. The thermal radiation and viscous dissipation have tendency to augment the Cu-water temperature over the stretching sheet.

1. INTRODUCTION

Now days, the demand for high-performance and proficient coolants in numerous industrial processes related to automobiles, metallurgy, power production, electronics, medical, etc., encouraged the several researchers towards nanofluids. The traditional fluids such as water, polymer solutions, ethylene glycol, oils and other lubricants have poor characteristics of heat transfer as these fluids have limited thermal conductivity. To augment the thermal conductivity of these traditional fluids, the researchers switched towards the artificial fluids termed as nanofluids by submerging the micro/nano sized metal particles into the traditional fluids (base fluids). Foremost, Choi [1] proved that the thermal conductivity of traditional fluids can be radically augmented by suspending the macro/nano sized particles of metal uniformly into the traditional fluids. This concept incited many researchers towards nanofluids, and numerous investigations were carried out to analyze the applications and thermo-physical properties of nanofluids [2-12]. Further, the experimental or theoretical analysis of magnetohydrodynamic (MHD) flow over the permeable and non-permeable stretching sheets has been vigorously done by several researchers owing to its enormous relevance in modern industry such as in heat storage systems, oil recovery techniques, production of emollient, fiber and wire coating, elastic polymer substance, chemical equipment processing, thermal insulations, manufacturing of uniform and long metal parts, etc. It is noted that the pioneering work on the

hydromagnetic flow of fluid owing to deformation of plane surface was performed by Pavlov [13]. Further, this investigation was explored by Chakrabarti and Gupta [14] taking into the consideration of temperature distribution, which may find the applications in various technology and industry such as polymer technology and in metallurgical process that engross cooling of the continuous strips. Makinde et al. [15] explored the impact of buoyancy force, magnetic field and Brownian motion on the stagnation point nanofluid flow over the stretched sheet. Moreover, Hayat et al. [16] discussed the magneto three dimensional fluid flow permeated by an exponentially stretched sheet. Most recently, Khan [17] obtained the series solution to explore the impact of magnetic field and other various relevant parameters on the visco-elastic flow of fluid over the shrinking or stretching sheet.

The consequence of heat source and/or sink on the laminar boundary layer fluid flow over a permeable stretched sheet has been accounted by many researchers owing to its strong consequences on the heat transfer characteristics. Following this, similarity solutions of boundary layer fluid flow driven by the stretched sheet considering heat source/sink is obtained by Elbashbeshy [18], which reveals that the suction can act as a medium for the cooling of moving continuous surface. Moreover, Elbashbeshy and Bazid [19] extended this study considering the unsteady boundary layer flow. Most recently, Ibrahim et al. [20] studied the impact of Cattaneo-Christov heat flux on the flow of UCM fluid past a melting surface under the influence of exponentially decaying heat

source/sink. Makinde et al. [21-22] discussed the magnetohydrodynamic mixed convective nanofluid flow over a permeable stretched sheet. It may be noted that many industrial processes like designing of furnace, solar power technology, production of glass, electrical power generation, propulsion devices for missiles and aircraft, etc. occurs at typically high temperature wherein the role of thermal radiation is noteworthy for surface heat transfer. Moreover, in the current circumstances, at a rapid pace the diminution of existing sources of conventional energy has drawn the attention to switch in the direction of renewable and sustainable energy sources for many industrial applications. The main source of renewable energy is the solar energy and the thermal radiation may act crucial part to convert the solar energy to the suitable form for the various industrial and scientific applications. For this reason, countless researchers have explored the consequences of radiative heat transfer on the boundary layer fluid flow over the plate/stretched sheet [23-26].

It is observed that the impact of viscous dissipation has not been accounted in aforementioned studies. Even though the viscous dissipation impact is presumed to be limited, but it's consequences in food processing, polymer manufacturing, instrumentations, lubrications etc. become significant because it amends the temperature distribution characteristics by acting like a typical energy source which tends to influence the rate of heat transfer. Some relevant investigations considering the viscous dissipation permeated by the stretched sheet are reported [27-30]. In addition to viscous dissipation's behavior, the Joule dissipation behaves like volumetric heat source in the hydromagnetic flows. In particular, the combined Joule and viscous dissipations influence are important in the heat treated materials confined among the nourished and wind-up rolls. Due to this reason, many researchers including of Anjali Devi and Ganga [31], Pal [32], Seth and Singh [33] and Seth et al. [34-35], etc. considered the combined influence of viscous and Joule dissipations. Most recently, Seth et al. [36] discussed the impact of Joule dissipation on the magneto-Casson fluid flow considering thin film over the horizontal stretched sheet.

However, in above discussed studies, the analytical/numerical solutions are analyzed assuming the no-slip boundary condition. But there are various physical situations like low pressure flows, nano/micro-scale flows etc. in which this boundary condition is not applicable. The phenomenon of non-adherence of fluids to the solid boundary is noticed under certain situations and is recognized as velocity slip. In the case of coated surface viz. resist adhesion and Teflon, no-slip condition is converted to Navier's partial slip in which the velocity slip is directly proportional to surface property and local shear stress. Following this, Mukopadhyay and Gorla [37] investigated significance of partial slip and radiative heat transfer on the boundary layer flow induced by porous exponentially stretched sheet. Moreover, Mukhopadhyay [38] discussed the impacts of partial slip on hydromagnetic and thermal radiative boundary layer flow considering suction/blowing over an exponentially stretched sheet. Sharma et al. [39] obtained the numerical solution of partial slip boundary layer and radiative flow of nanofluid with heat transfer over stretched sheet and discussed the influence of flow parameters in details.

In present study, our intent is to examine the impact of thermal radiation on viscous dissipative boundary layer flow of magneto-nanofluid with heat absorption over a permeable

exponentially stretching sheet considering Navier's velocity and thermal slips into account. To the best of our information, no one has attempted this problem which may find the applications in polymer technology and in metallurgical process that engross cooling of the continuous strips.

2. MATHEMATICAL ANALYSIS

2.1 Mathematical formulation of problem

The steady two-dimensional viscous dissipative boundary layer flow of an optically thick heat radiative, electrically conducting and incompressible magneto-nanofluid over a permeable exponentially stretched sheet is considered. The stretching sheet is aligned with x -axis whereas y -axis is taken in normal direction and flow of fluid being restricted to $y > 0$. The fluid is infused over the permeable exponentially stretched sheet owing to the velocity $\lambda_1(x)$. The nanofluid is permeated by uniform magnetic field B_0 exerted normal to the permeable stretched sheet. At the surface of stretched, the temperature is presumed to be constant given by \bar{T}_e while those of ambient nanofluid is considered as \bar{T}_∞ . The schematic representation of problem is displayed in Figure 1. Three kinds of water based nanofluids comprising of aluminum oxide, copper and titanium oxide as nanoparticles and its influence are taken into account. Further, both nanoparticles and base fluid are in thermal equilibrium and no slip mechanism occurs between them. Moreover, very small magnetic Reynolds number is considered to neglect induced magnetic field. The thermo-physical characteristics of water and the considered nanoparticles are shown in Table 1.

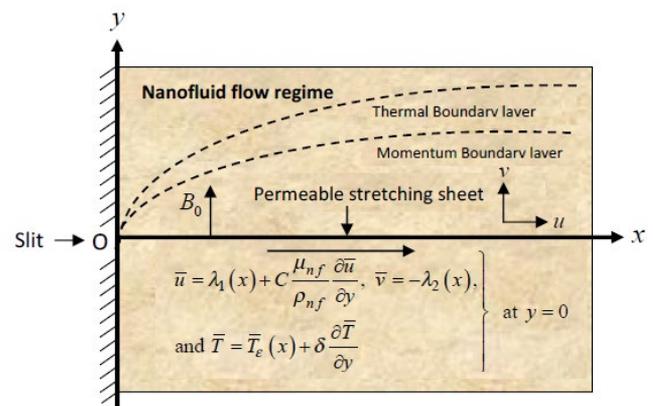


Figure 1. The schematic representation of problem

Table 1. Thermo physical characteristics of base fluid and nanoparticles [40]

	TiO ₂	Al ₂ O ₃	Cu	Water
ρ (kg/m ³)	4250	3970	8933	997.1
c_p (J/kg K)	686.2	765	385	4179
k (W/m K)	8.9538	40	401	0.613
ϕ	0.20	0.15	0.05	0.00
σ ($\Omega \cdot m$) ⁻¹	1×10^{-12}	1×10^{-10}	59.6×10^6	0.05

Owing to aforesaid assumptions, the governing mathematical equations of the problem are given by

$$\frac{\partial \bar{u}}{\partial x} + \frac{\partial \bar{v}}{\partial y} = 0, \quad (1)$$

$$\bar{u} \frac{\partial \bar{u}}{\partial x} + \bar{v} \frac{\partial \bar{u}}{\partial y} = \frac{\mu_{nf}}{\rho_{nf}} \frac{\partial^2 \bar{u}}{\partial y^2} - \frac{\sigma_{nf} B_0^2}{\rho_{nf}} \bar{u}, \quad (2)$$

$$\begin{aligned} \bar{u} \frac{\partial \bar{T}}{\partial x} + \bar{v} \frac{\partial \bar{T}}{\partial y} &= \frac{k_{nf}}{(\rho c_p)_{nf}} \frac{\partial^2 \bar{T}}{\partial y^2} + \frac{\mu_{nf}}{(\rho c_p)_{nf}} \left(\frac{\partial \bar{u}}{\partial y} \right)^2 \\ &- \frac{1}{(\rho c_p)_{nf}} \left\{ \frac{\partial q_r}{\partial y} - \sigma_{nf} B_0^2 \bar{u}^2 + Q_0 (\bar{T} - \bar{T}_\infty) \right\}. \end{aligned} \quad (3)$$

As per the assumptions, the allied boundary conditions are presented by

$$\left. \begin{aligned} \bar{u} &= \lambda_1(x) + C \frac{\mu_{nf}}{\rho_{nf}} \frac{\partial \bar{u}}{\partial y}, \quad \bar{v} = -\lambda_2(x), \\ \bar{T} &= \bar{T}_\varepsilon(x) + \delta \frac{\partial \bar{T}}{\partial y} \end{aligned} \right\} \text{at } y = 0, \quad (4a)$$

$$\bar{u} \rightarrow 0, \quad \bar{T} \rightarrow \bar{T}_\infty \quad \text{as } y \rightarrow \infty, \quad (4b)$$

where $\lambda_1(x) = \lambda_0 e^{x/2L}$ is the velocity of stretched sheet, $\bar{T}_\varepsilon(x) = (\bar{T}_0 - \bar{T}_\infty) e^{\delta_0 x/2L} + \bar{T}_\infty$ is exponential nanofluid temperature distribution in the sheet, λ_0 and \bar{T}_0 are the velocity reference and temperature respectively, δ_0 is the temperature distribution parameter within the stretched sheet, $C = C_1 e^{-x/2L}$ is used for velocity slip factor wherein C_1 represents the initial velocity slip value, $\delta = \delta_1 e^{-x/2L}$ signifies the thermal slip factor in which δ_1 shows the initial thermal slip factor. Both velocity and thermal slip factors change along with the variable x . Meanwhile, no-slip occurs for $C = \delta = 0$. Here $\lambda_2(x) = v_0 e^{x/2L}$ indicates the suction/blowing velocity and v_0 is the suction/blowing velocity initial strength.

The expressions of $\rho_{nf}, \sigma_{nf}, (\rho c_p)_{nf}$ and μ_{nf} for the nanofluid are defined [41-42] as

$$\left. \begin{aligned} \rho_{nf} &= \rho_f \left\{ (1-\phi) + \phi \frac{\rho_s}{\rho_f} \right\}, \quad \sigma = \frac{\sigma_s}{\sigma_f}, \\ \sigma_{nf} &= \sigma_f \left[\frac{3(\sigma-1)\phi}{(\sigma+2) - (\sigma-1)\phi} + 1 \right], \\ (\rho c_p)_{nf} &= (\rho c_p)_f \left\{ (1-\phi) + \phi \frac{(\rho c_p)_s}{(\rho c_p)_f} \right\}, \\ \mu_{nf} &= \mu_f (1-\phi)^{-5/2}. \end{aligned} \right\} \quad (5)$$

It may be noted that the abovementioned expressions (5) are constrained to spherical nanoparticles while it is not applicable for the nanoparticles having the other shape [40]. Further, for the nanofluid comprising of spherical shape nanoparticles the effective thermal conductivity k_{nf} is given as

$$k_{nf} k_f^{-1} = \left\{ \frac{k_s - 2(k_f - k_s)\phi + 2k_f}{k_s + (k_f - k_s)\phi + 2k_f} \right\}, \quad (6)$$

where k_f and k_s , k_f and k_s are, respectively, the thermal conductivities of water and nanoparticles.

The Rosseland approximation is considered for optically thick radiative fluid [43] to express the radiative heat flux q_r in the following form

$$q_r = -\frac{4\sigma^*}{3k^*} \frac{\partial \bar{T}^4}{\partial y}. \quad (7)$$

Moreover, \bar{T}^4 is linearized by expanding it about the free stream temperature \bar{T}_∞ using the Taylor's series, which is represented below after neglecting the higher order terms

$$\bar{T}^4 \cong 4\bar{T}_\infty^3 \bar{T} - 3\bar{T}_\infty^4. \quad (8)$$

Now using (7) and (8) in equation (3), we get

$$\begin{aligned} \bar{u} \frac{\partial \bar{T}}{\partial x} + \bar{v} \frac{\partial \bar{T}}{\partial y} &= \frac{1}{(\rho c_p)_{nf}} \left[k_{nf} + \frac{16\sigma^* \bar{T}_\infty^3}{3k^*} \right] \frac{\partial^2 \bar{T}}{\partial y^2} + \frac{\mu_{nf}}{(\rho c_p)_{nf}} \left(\frac{\partial \bar{u}}{\partial y} \right)^2 \\ &+ \frac{1}{(\rho c_p)_{nf}} \left\{ \sigma_{nf} B_0^2 \bar{u}^2 - Q_0 (\bar{T} - \bar{T}_\infty) \right\}. \end{aligned} \quad (9)$$

2.2 Numerical solution of problem

For the physically reliable numerical solution of aforesaid problem, following similarity transforms [44] have been introduced

$$\begin{aligned} \psi(x, y) &= \sqrt{2Re} e^{x/2L} v_f f(\eta), \quad \eta(x, y) = \frac{y}{L} \sqrt{\frac{Re}{2}} e^{x/2L} \\ \text{and } \bar{T}(x, y) &= e^{\delta_0 x/2L} (\bar{T}_0 - \bar{T}_\infty) \theta(\eta) + \bar{T}_\infty, \end{aligned} \quad (10)$$

where v_f, Re, ψ, η and θ represent the fluid kinematic viscosity, Reynolds number, stream function, similarity variable and dimensionless form of nanofluid temperature respectively where ψ (stream function) is defined by the following relations

$$\bar{u} = \frac{\partial \psi}{\partial y} \quad \text{and} \quad \bar{v} = -\frac{\partial \psi}{\partial x}. \quad (11)$$

Now using equation (10) in (11), we get

$$\left. \begin{aligned} \bar{u} &= \frac{Re v_f}{L} e^{x/2L} f'(\eta) \quad \text{and} \\ \bar{v} &= -\frac{\sqrt{2Re} v_f}{2L} [f(\eta) + \eta f'(\eta)] e^{x/2L}, \end{aligned} \right\} \quad (12)$$

where primes indicate the differentiation with respect to η . The equations (10) and (11) transform the equations (2) and (9) into the set of non linear ordinary equations:

$$\phi_1 f''' + \phi_2 (f'' f - 2f'^2) - 2\phi_3 Me^{-X} f' = 0, \quad (13)$$

$$\left(\frac{K_1 + R}{Pr\phi_4}\right)\theta'' + f\theta' - \delta_0\theta f' + Ec\left(\phi_1 e^{X} f'^2 + 2\phi_3 M f'^2\right)e^{(2-\delta_0)X/2} - \frac{2\xi}{\phi_4} e^{-X}\theta = 0, \quad (14)$$

with the associated boundary conditions in dimensionless forms as obtained from the equations (4a) and (4b) in the following form

$$f' = 1 + \lambda_3 f'', \quad f = S \quad \text{and} \quad \theta = 1 + \delta_2 \theta' \quad \text{at} \quad \eta = 0, \quad (15a)$$

$$f' \rightarrow 0 \quad \text{and} \quad \theta \rightarrow 0 \quad \text{as} \quad \eta \rightarrow \infty, \quad (15b)$$

where $X = xL^{-1}$ is the dimensionless coordinate. The dimensionless parameters appearing in the equations (13)-(15b) are

$$\left. \begin{aligned} M &= \frac{\sigma_f (B_0 L)^2}{Re\mu_f}, \quad Pr = \frac{(\rho\nu c_p)_f}{k_f}, \quad R = \frac{16\sigma^* \bar{T}_\infty^3}{3k^* k_f}, \quad Re = \frac{\lambda_0 L}{\nu_f}, \\ Ec &= \frac{\lambda_0^2}{(c_p)_f (\bar{T}_0 - \bar{T}_\infty)}, \quad \xi = \frac{Q_0 L^2}{\rho_f \nu_f (c_p)_f Re}, \quad \lambda_3 = \frac{C_1 \mu_{nf} \sqrt{Re}}{L \rho_{nf}}, \\ \delta_2 &= \frac{\delta_1}{L} \sqrt{\frac{Re}{2}} \quad \text{and} \quad S = \frac{\nu_0 L}{\nu_f} \sqrt{\frac{2}{Re}}. \end{aligned} \right\} \quad (16)$$

Also, we have

$$\left. \begin{aligned} \phi_1 &= \frac{1}{(1-\phi)^{2.5}}, \quad \phi_2 = \frac{1}{\rho_f} \left\{ (1-\phi)\rho_f + \phi\rho_s \right\}, \\ \phi_3 &= \frac{(\sigma+2) + 2(\sigma-1)\phi}{(\sigma+2) - (\sigma-1)\phi}, \quad \phi_4 = \left\{ (1-\phi) + \phi \frac{(\rho c_p)_s}{(\rho c_p)_f} \right\} \\ \text{and } K_1 &= \left\{ \frac{k_s - 2(k_f - k_s)\phi + 2k_f}{k_s + (k_f - k_s)\phi + 2k_f} \right\}. \end{aligned} \right\} \quad (17)$$

2.3 Skin friction coefficient and local Nusselt number

For the engineering interest, the skin friction coefficient Cf_x and local Nusselt number Nu_x are, respectively, given by

$$Cf_x = \tau_w \left\{ \rho_f \lambda_1^2(x) \right\}^{-1} \quad \text{and} \quad Nu_x = x q_w \left\{ k_f (\bar{T}_\varepsilon - \bar{T}_\infty) \right\}^{-1}, \quad (18)$$

where $\tau_w = \mu_{nf} (\partial u / \partial y)_{y=0}$ and $q_w = -k_{nf} (\partial \bar{T} / \partial y)_{y=0} + (q_r)_{y=0}$ are the wall shear stress and wall heat flux respectively. The non-dimensional form of local skin friction coefficient and local Nusselt numbers are represented as

$$\left. \begin{aligned} Cf_x &= \phi_1 Re_x^{-1/2} \sqrt{2X} f''(0) \quad \text{and} \\ Nu_x &= -K_1 \left\{ (1+R) Re_x^{1/2} (X/2)^{1/2} \right\} \theta'(0), \end{aligned} \right\} \quad (19)$$

where $Re_x = x\lambda_1(x)/\nu_f$ is the local Reynolds number.

3. IMPLEMENTATION OF NUMERICAL METHOD FOR THE SOLUTION

The solution of equations reported in section 2.2 cannot be obtained analytically owing to the coupled nature of non-linear equations. Therefore, the numerical solutions of these equations along with the associated boundary conditions are obtained using shooting technique in conjunction with Runge-Kutta method of fourth order. Foremost, the prevailing equations (13) and (14) are changed into the set of highly coupled form of five first order non linear differential equations. To solve these set of equations by Runge-Kutta scheme of fourth order, the initial values of $f''(0)$ and $\theta'(0)$ are needed. So, the initial guess values for $f''(0)$ and $\theta'(0)$ are obtained using shooting technique. Further, these initial guess values are corrected with the help of Secant method. During the numerical computation step size is considered as 0.001 and the value of $\eta = 17$ is considered for the associated boundary condition 15(b). In order to achieve the precise results the entire process is repeated wherein the tolerance error is considered as 10^{-6} .

4. RESULTS AND DISCUSSION

Extensive numerical computation is performed for the nanofluid velocity $f'(\eta)$, nanofluid temperature $\theta(\eta)$, skin friction coefficient Cf_x and wall temperature gradients using Runge-Kutta method of fourth order along with the shooting scheme. The computed numerical results are presented to illustrate a parametric study enumerating impacts of pertinent flow parameters on the flow field. Three kinds of water based nanofluids having titanium oxide, alumina and copper as nanoparticles are chosen for this investigation. Throughout the study, dimensionless physical parameters are considered as $X = 1.5, a = 2, M = 0.2, \phi = 0.05, S = 0.1, \lambda_3 = 0.3, \delta_2 = 0.1, Ec = 0.1, R = 0.1, \xi = 0.1$ and $Pr = 6.2$ (for base fluid) unless stated otherwise. The nanofluid velocity and temperature distribution profiles for the three kinds of nanofluids consisting of Cu, Al_2O_3 , TiO_2 as nanoparticles and water as base fluid over the exponentially stretching sheet are displayed in Figures 2a and 2b. It is noticed that Cu-water nanofluid has lower velocity and temperature profiles followed by Al_2O_3 -water and TiO_2 -water nanofluids in the regime of boundary layer. Further, it is also noted that these profiles nearly overlap with each other away from the stretching sheet for the precise values of pertinent flow parameters. Figures 3a and 3b depict the significance of volume fraction of nanoparticle ϕ on the Cu-water nanofluid velocity $f'(\eta)$ and nanofluid temperature $\theta(\eta)$. These figures inferred that the velocity of nanofluid gets retarded while temperature is enhanced due to augmentation of numeric values of ϕ . This is because of the fact that enhancement in volume fraction of nanoparticle leads to thermal conductivity reduction of nanofluid which results the boundary layer thickness to decrease and viscosity to enhance and in turn the nanofluid velocity gets reduced and fluid temperature gets enhanced. The consequences of magnetic parameter M on the profiles of velocity and temperature for Cu-water nanofluid are displayed in Figures 4a and 4b. It is revealed that the nanofluid velocity gets slow down whereas temperature of fluid is enhanced on augmenting M . This tendency of magnetic field is justified because it produces an opposing

force (i.e. Lorentz force), which works in opposite direction to the fluid flow and metal nanoparticles and as a result fluid velocity is retarded and fluid temperature gets enhanced.

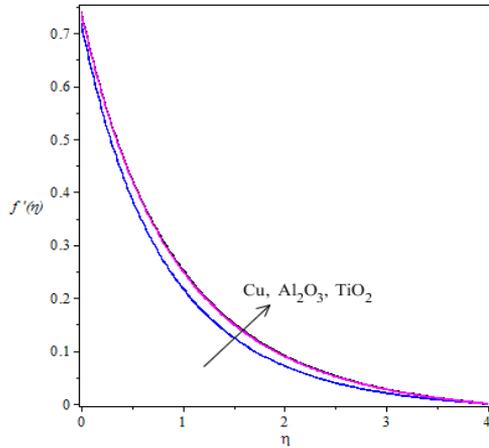


Figure 2a. Velocity profiles comparison for the different nanofluids

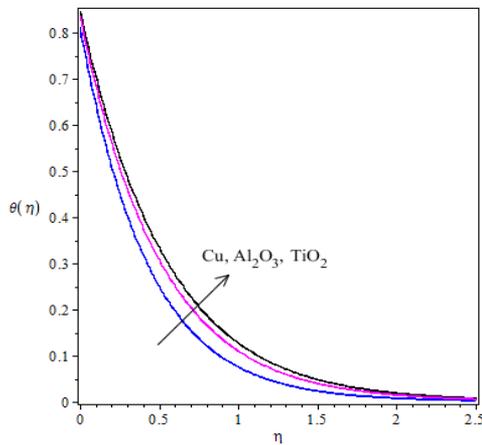


Figure 2b. Temperature distribution profiles comparison for the different nanofluids

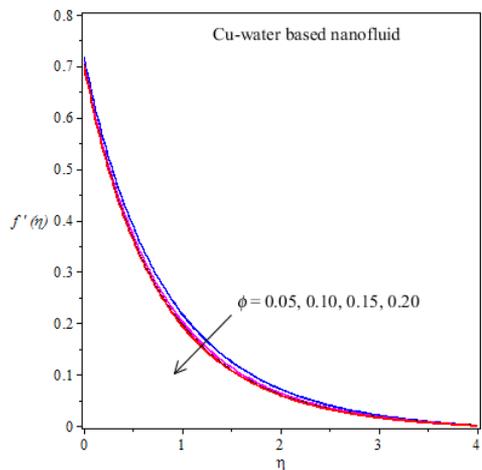


Figure 3a. Velocity profiles variation for varying values of ϕ

Figures 5a and 5b portray the influence of non-dimensional coordinate X on the Cu-water nanofluid velocity profiles and temperature distribution. These figures illustrate that both the nanofluid velocity $f'(\eta)$ and temperature $\theta(\eta)$ get enhanced on increasing X which implies that the non-dimensional coordinate X has enhancing effect on both nanofluid velocity and temperature in the regime of boundary

layer.

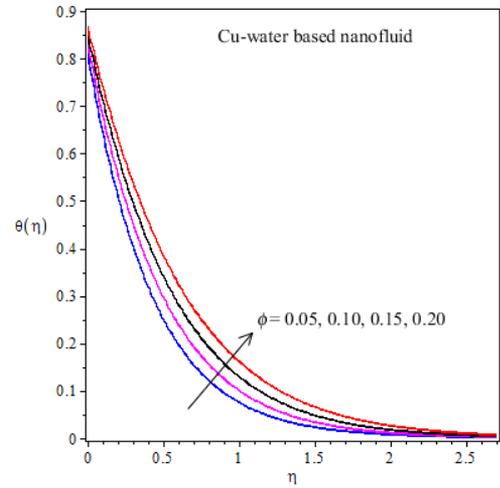


Figure 3b. Temperature profiles variation for varying values of ϕ

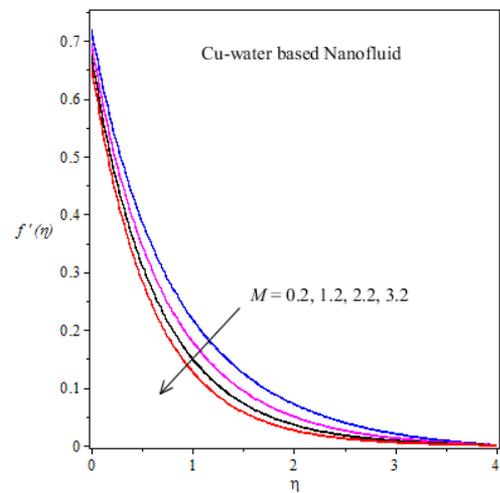


Figure 4a. Velocity profiles variation for varying values of M

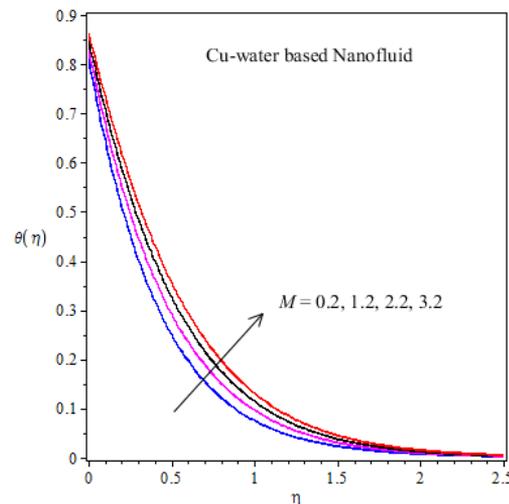


Figure 4b. Temperature profiles variation for varying values of M

Figures 6a and 6b quantify the significance of velocity slip factor on the flow field. These figures emphasize that the nanofluid velocity is retarded whereas fluid temperature gets augmented due to velocity slip parameter λ_3 . This phenomena

is due to the reason that in the proximity of sheet both fluid and stretching sheet velocities are not same when slip occurs and as a result the fluid velocity gets diminished with increase in velocity slip factor parameter because in the existence of slip condition pulling of stretching is partially transmitted to fluid, which reveals that the velocity slip has significant impact on the flow of fluid. Figures 7a and 7b inferred the diminishing impact on the profiles of both nanofluid velocity and temperature for suction parameter $S(> 0)$ while it has a reversal effect on increasing the injection parameter $S(< 0)$. This phenomena is owing to the reason that the momentum boundary layer during suction sticks very close to the stretching sheet, which demolish the flow momentum and as a result nanofluid fluid velocity gets reduced while injection appends fluid by means of lateral mass flux over the sheet which tends to assist the momentum of flow and consequently the fluid velocity gets augmented. Figure 8 demonstrates the thermal radiation effect on the nanofluid temperature. It is clear that the Cu based nanofluid temperature is enhanced due to rising of thermal radiation parameter because it increases the conduction effect of the fluid and consequently thermal boundary layer turn into thicker. The consequence of viscous dissipation on Cu based fluid temperature is show in Figure 9. It is noticed that the increasing values of Ec leads to enhancement in the fluid temperature. This implies that the viscous dissipation tends to augment the nanofluid temperature in the regime of boundary layer.

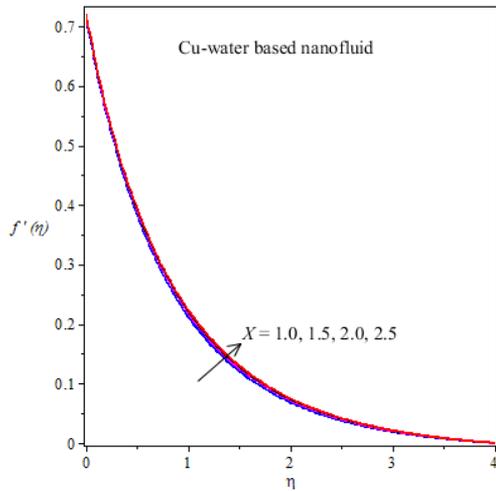


Figure 5a. Velocity profiles variation for varying values of X

Figures 10a and 10b exemplify the impacts of M , ϕ and X on the wall velocity gradient and local Nusselt number Nu_x . These figures signify that an increase in either M or ϕ leads to reduce the skin friction coefficient $|Cf_x|$ while it is enhanced due to amplification of dimensionless coordinate X . Further, the local Nusselt number Nu_x gets augmented due to intensification of M , ϕ and X . Figures 11a and 11b reckon the significance of suction/injection parameter S and velocity slip parameter λ_3 on skin friction coefficient and local Nusselt number. It is interesting to mention that both skin friction coefficient and local Nusselt number in magnitude increase due to enhancement in injection and velocity slip parameters while both decrease on increasing the suction parameter. Physically, it is interoperated that due to injection and velocity slip factor both shear stress and rate of heat transfer get enhanced at the

stretched sheet whereas suction has a reversal impact. From Figure 12, it is noticed that the magnitude of local Nusselt number increases due to amplification of Eckert number Ec , radiation parameter R and thermal slip parameter δ_2 . This implies that viscous dissipation, thermal radiation and thermal slip have propensity to augment the rate of wall temperature gradient over the stretching sheet.

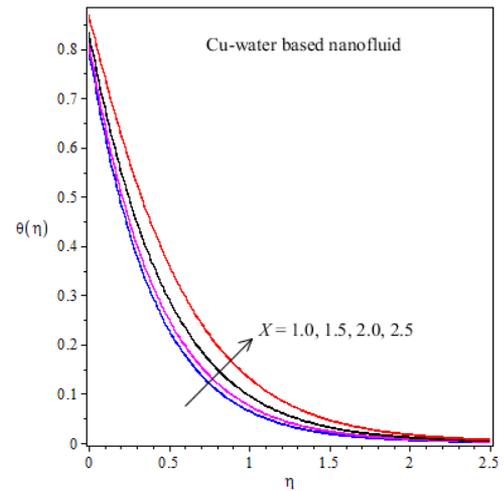


Figure 5b. Temperature profiles variation for varying values of X

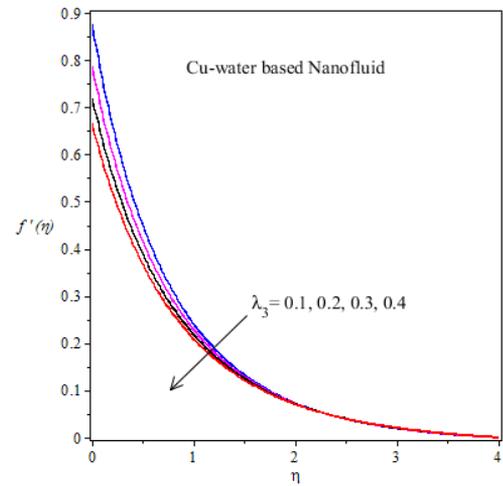


Figure 6a. Velocity profiles variation for varying values of λ_3

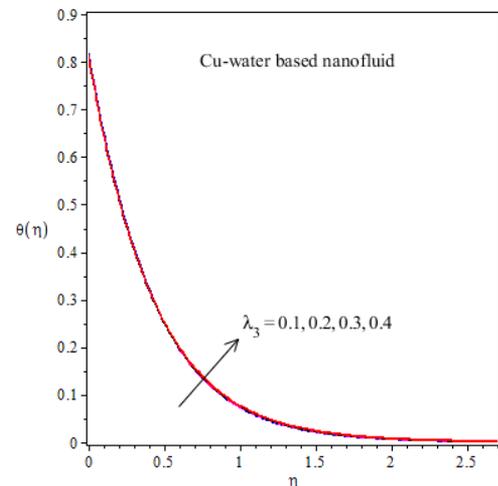


Figure 6b. Temperature profiles variation for varying values of λ_3

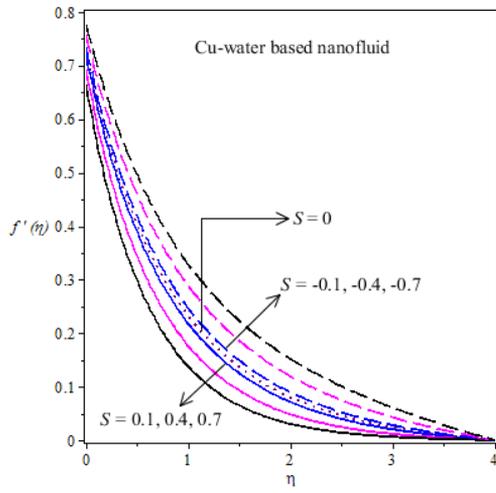


Figure 7a. Velocity profiles variation for varying values of S

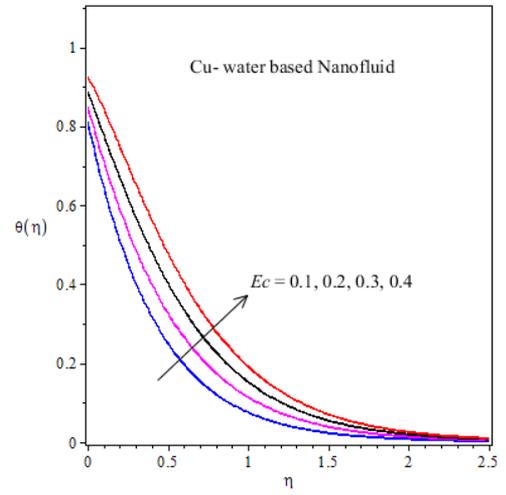


Figure 9. Temperature profiles variation for varying values of Ec

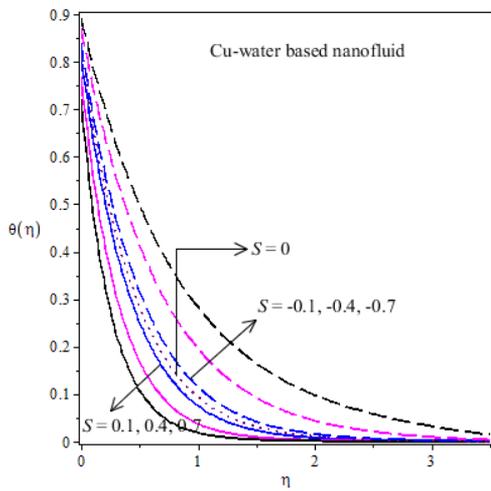


Figure 7b. Temperature profiles variation for varying values of S

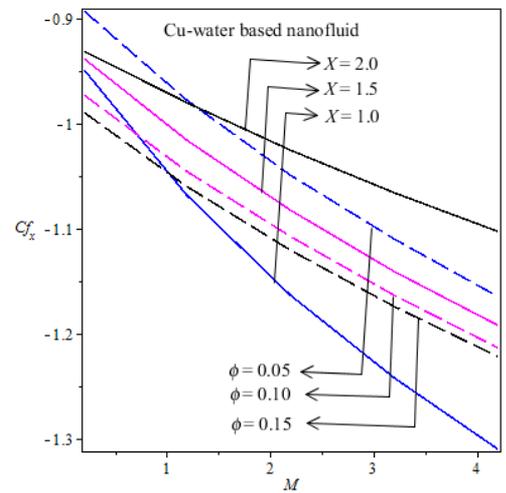


Figure 10a. Profiles of Cf_x for varying values of X , ϕ and M

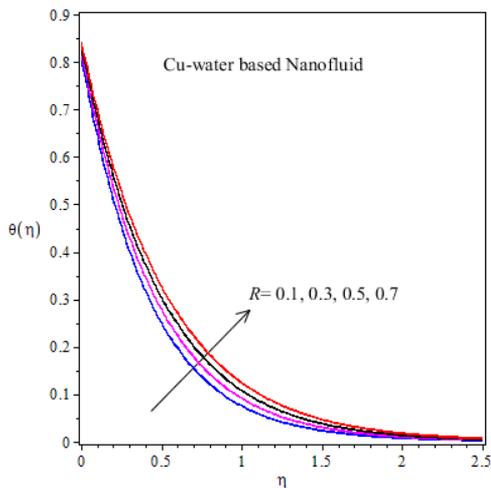


Figure 8. Temperature profiles variation for varying values of R

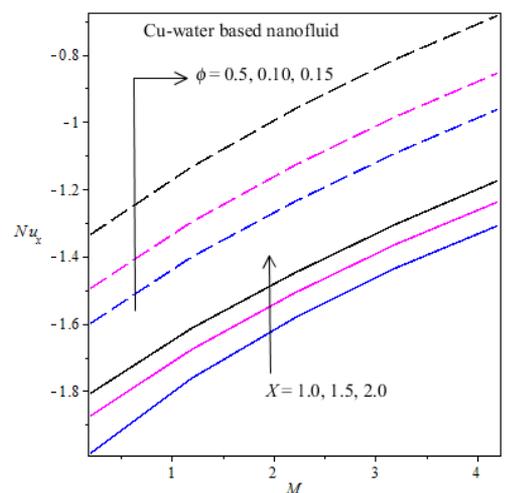


Figure 10b. Profiles of Nu_x for varying values of X , ϕ and M

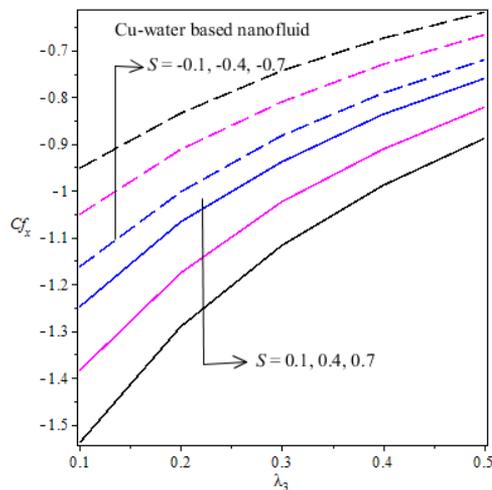


Figure 11a. Profiles of Cf_x for varying values of S and λ_3

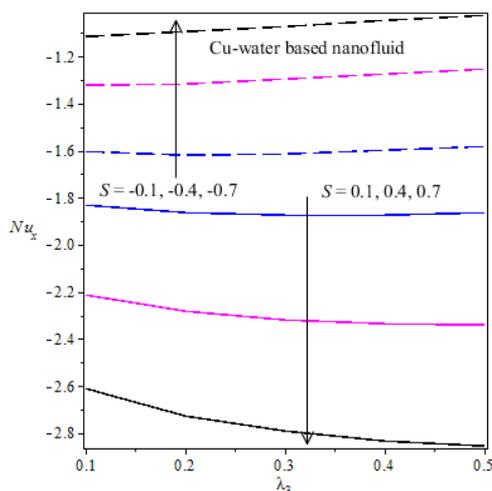


Figure 11b. Profiles of Nu_x for varying values of S and λ_3

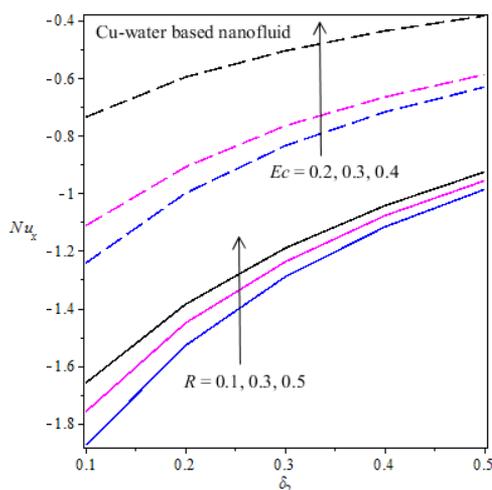


Figure 12. Profiles of Nu_x for varying values of Ec , R and δ_2

5. VALIDATION OF IMPLEMENTED NUMERICAL METHOD

The accuracy of numerical algorithm implemented in our study has been validated by comparing the numerical values

of local Nusselt number Nu_x with existed limiting results of Rashidi et al. [45] when $X = \delta_0 = S = \lambda_3 = \delta_2 = Ec = \xi = 0$, $\phi = 0.05$, $R = 0.1$ and $Pr = 6.2$ and Pal [32] when $X = 1.5$, $S = \lambda_3 = \delta_2 = R = \phi = 0$, $\delta_0 = 2$, $Ec = 0.1$, $\xi = 0.1$ and $Pr = 6.2$. The comparison of both the results reveals an excellent conformity of present results as it is evident from Table 2, which accentuates the correctness of the implemented numerical algorithm.

Table 2. Comparison of numerical values of Nu_x i.e. local Nusselt number with the previous results reported by Rashidi et al. [45] and Pal [32]

M	Rashidi et al. [45]	Pal [32]	Present result
0.5	-1.401345	-1.40134	-1.401347
1.5	-1.291168	-1.29116	-1.291166
2.5	-1.206645	-1.20664	-1.206645
3.5	-1.138282	-1.13828	-1.138281

6. QUADRATIC REGRESSION ESTIMATION

Quadratic regression analysis is one kind of statistical technique for estimating the relationship of the variables. More precisely, regression analysis plays a significant role to comprehend how the particular value of a dependent variable varies due to change of an independent variable keeping other independent variables fixed. In this section, an analysis of quadratic regression estimation for the skin friction coefficient Cf_x and local Nusselt number Nu_x has been presented. The estimated numerical values of Cf_x and Nu_x have been computed for 125 sets of various values of S and λ_3 taken from the intervals $[0.5, 3]$ and $[0.05, 0.50]$, respectively, whereas other parameters are considered fixed as mentioned.

The quadratic regression estimated model for Cf_x and Nu_x are mentioned below

$$Cf_{qre} = Cf_x + b_1S + b_2\lambda_3 + b_3S^2 + b_4\lambda_3^2 + b_5S\lambda_3, \quad (20)$$

$$Nu_{qre} = Nu_x + c_1S + c_2\lambda_3 + c_3S^2 + c_4\lambda_3^2 + c_5S\lambda_3, \quad (21)$$

where b_1, b_2, b_3, b_4 and b_5 are the coefficients skin friction estimations and c_1, c_2, c_3, c_4 and c_5 are coefficients of local Nusselt number estimations.

The coefficients of quadratic regression estimation corresponding to skin friction coefficient Cf_x and local Nusselt number Nu_x are presented in Tables 3 and 4 for different values of magnetic parameter M and volume fraction of nanoparticle ϕ . Moreover, the maximum values of relative error bounds $\varepsilon_1 = |Cf_{qre} - Cf_x|/Cf_x$ and $\varepsilon_2 = |Nu_{qre} - Nu_x|/Nu_x$ are also computed. These tables indicate that the coefficients of λ_3 are greater as compared to S which reveal that small change in λ_3 leads in a maximum perturbation in both the shear stress and rate of heat transfer at the stretched sheet. This suggests that the velocity slip factor has augmenting impact on both the wall velocity gradient and rate of heat transfer at the stretched sheet. This observation is also justified from Figures 11a and 11b.

Table 3. Estimated quadratic regression coefficients and relative error bounds of Cf_x for varying M and ϕ

M	ϕ	Cf_x	b1	b2	b3	b4	b5	ϵ_1
0.2	0.05	-1.3959	-0.5845	2.7321	0.0014	-1.9956	1.1241	0.0202
0.2	0.15	-1.5060	-0.6970	3.1769	0.0087	-2.3746	1.3743	0.0229
2.2	0.05	-1.6721	-0.5630	3.3107	0.0083	-2.5384	1.1014	0.0157
2.2	0.15	-1.7632	-0.6704	3.7293	0.0145	-2.9066	1.3417	0.0183

Table 4. Estimated quadratic regression coefficients and relative error bounds of Nu_x for varying M and ϕ

M	ϕ	Nu_x	c1	c2	c3	c4	c5	ϵ_2
0.2	0.05	1.6716	1.3010	0.8284	-0.0426	-0.5380	0.9506	0.0188
0.2	0.15	1.2171	0.8133	1.4702	0.0655	-1.2130	1.1356	0.0299
2.2	0.05	1.1032	1.5575	1.9188	-0.0551	-0.9994	0.9473	0.0500
2.2	0.15	0.6162	1.0985	2.7008	0.0456	-1.8575	1.0880	0.1049

7. CONCLUSIONS

In this study, we have examined the impact of thermal radiation on viscous dissipative boundary layer flow of heat absorbing magneto-nanofluid over a permeable exponentially stretching sheet considering Navier's velocity and thermal slips into account. Three kinds of water based nanofluids having alumina (Al_2O_3), copper (Cu) and titanium oxide (TiO_2) as nanoparticles are chosen for this investigation. Numerical computations are performed for various physical parameters and their significance on the flow field is quantified through numerous graphs. The quadratic regression analysis on the numerical data of Cf_x and Nu_x has been presented to verify the relationship among the controlling physical parameters and transfer rate parameters. The implemented numerical algorithm has been validated by comparing the numerical values of Nu_x with existed limiting results considering special assumptions. Following significant findings are drawn from various figures and tables:

- (i) The velocity and temperature distribution profiles are lower for Cu-water nanofluid followed by Al_2O_3 and TiO_2 water base nanofluids in the regime of boundary layer.
- (ii) The volume fractions of nanoparticle, exerted magnetic field and velocity slip factor have diminishing impact on the velocity and augmenting impact on the temperature profiles for Cu-water nanofluid.
- (iii) Both the Cu-water fluid velocity and temperature are increased due to injection parameter where suction parameter has reversal impact.
- (iv) The viscous dissipation and thermal radiation have tendency to augment the Cu-water temperature over the stretching sheet.
- (v) In case of Cu based nanofluid, the shear stress at the stretching sheet is reduced whereas rate of heat transfer is enhanced due to amplification of magnetic parameter, volume fraction of nanoparticle.
- (vi) Viscous dissipation, thermal slip factor and thermal radiation have propensity to augment the heat transfer rate over the stretched sheet for Cu-water nanofluid.

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NOMENCLATURE

Ec	Eckert number
k^*	Rosseland mean absorption coefficient
k_{nf}	Thermal conductivity of nanofluid
M	Magnetic parameter
Pr	Prandtl number
q_r	Radiative heat flux
R	Radiation parameter
Re	Reynold's number
S	Suction / injection parameter
\bar{T}	Temperature of nanofluid
\bar{u}	Nanofluid velocity along x-axis
\bar{v}	Nanofluid velocity along y-axis

Greek symbols

δ_2	Thermal slip parameter
λ_3	Velocity slip parameter
μ_f	Base fluid dynamic viscosity
μ_{nf}	Dynamics viscosity of nanofluid
ξ	Heat absorption parameter
ρ_f	Base fluid density
ρ_{nf}	Nanofluid density
ρ_s	Nanofluid density
$(\rho c_p)_f$	Base fluid's heat capacitance
$(\rho c_p)_{nf}$	Heat capacitance of nanofluid
$(\rho c_p)_s$	Heat capacitance of nanoparticles
σ^*	Stefan Boltzmann constant
σ_f	Base fluid electrical conductivity
σ_{nf}	Nanofluid electrical conductivity
σ_s	Nanofluid electrical conductivity
ϕ	Volume fraction of nanoparticles