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# Twelve Sectors DPC Control Based on Neural Hysteresis Comparators of the DFIG Integrated to Wind Power

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ABSTRACT

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A twelve sectors direct power control (TSDPC) drive allows direct and independent command of reactive power linkage and active power by the selection of optimum inverter switching tables (STs). There is no need for any complex transformation of voltage or current. However, each vector selected from the ST cannot produce the required accurate rotor voltage vector (VV) to provide the desired reactive and active power. This results in the production of ripples in the reactive power as well as active power waveforms. In this study, we propose a technique to minimize active and reactive power ripples. In this technique, the hysteresis comparators are replaced by two artificial neural networks (ANNs) controller and are compared to the TSDPC technique. The traditional twelve sectors DPC and the proposed technique are simulated and the comparison of their performances is presented.

#### **1. INTRODUCTION**

The doubly-fed induction generator (DFIG) is a widely used in wind energy conversion system (WECS). The major advantages of three-phase DFIGs are as follows: simple control, robust and rotor side converter is only sized for 30% power compared to synchronous generators (SGs) based WECS [1]. Various techniques have been proposed for controlling the DFIG. Five-level direct power control (DPC) scheme based on a neural algorithm has been proposed [2]. Direct vector control (DVC) strategy were proposed based on neural space vector pulse width modulation (NSVPWM), where the hysteresis comparators was replaced by a neural algorithm [3]. Twelve sectors DPC technique is proposed to control DFIG-WECS [4]. Indirect vector control (IVC) based on the fuzzy SVPWM (FSVPWM) strategy has been proposed [5]. A neuro-sliding mode controller (NSMC) was designed to control the DFIG by using neural pulse width modulation (NPWM) [6]. The stator active/reactive power ripple reduced by using fuzzy SMC (FSMC) [7]. A neuro-second order sliding mode controller (NSOSMC) is proposed to minimize the active/reactive power ripple of the DFIG-based wind turbines [8, 9]. SOSMC and fuzzy logic techniques are combined to control the DFIG [10]. Direct torque control (DTC) based on neural proportional-integral (PI) controllers and SVPWM technique [11]. SMC strategy and adaptive network-based fuzzy inference system (ANFIS) are combined to reducd harmonic distortion of stator current [12]. The SOSMC strategy based on the ANFIS algorithm has been proposed [13]. A DPC strategy based on the seven-level SVPWM technique has been proposed [14]. In this paper, we propose a new method of direct power control (DPC) by using two-level neural hysteresis comparators for active and reactive powers.

The main objective of this work is the studying of the conventional twelve sectors DPC method (TSDPC) and TSDPC with neural hysteresis comparators (TSDPC-NHC) applied to the doubly fed induction generator (DFIG) therefore; our work is organized as follows:

• The first part is devoted to the principal method of 12 sectors DPC is presented.

• In the second part, we present 12 sectors DPC of the DFIG by using NHC.

#### 2. TSDPC STRATEGY

Twelve sectors DPC strategy is based on applying a switching series, which shall directly eliminate errors, which shall occur in active/reactive power, through the reference given as value and the calculated active/reactive power, to the power switching elements in the inverter [15, 16]. The twelve sectors DPC method, which is designed to regulate the reactive/active power of the DFIG-based WECS, is shown in Figure 1 [17].

This may be realized by using the generator model on the fixed d-q axis set. Reactive power, active power, and rotor flux sector zone may be calculated with the help of currents and voltages measured in the generator rotor [18].

Stator active/reactive power is estimated using (1) and (2) [19].

$$P_{s} = -\frac{3}{2} \frac{L_{m}}{\sigma . L_{s} . L_{r}} \cdot (V_{s} . \psi_{r\beta})$$
(1)

$$Q_{s} = -\frac{3}{2} \left( \frac{V_{s}}{\sigma . L_{s}} \cdot \psi_{r\beta} - \frac{V_{s} . L_{m}}{\sigma . L_{s} . L_{r}} \cdot \psi_{r\alpha} \right)$$
(2)



Active and reactive power estimation

Figure 1. Twelve sectors DPC method

The active and reactive powers can be reformulated by inducing angle  $\lambda$  between the stator and rotor vectors as follows:

$$P_{s} = -\frac{3}{2} \frac{L_{m}}{\sigma . L_{s} . L_{r}} w_{s} |\psi_{s}| |\psi_{r}| \sin(\lambda)$$
(3)

$$Q_s = -\frac{3}{2} \frac{w_s}{\sigma L_s} |\psi_s| (\frac{M}{L_r} |\psi_r| \cos(\lambda) - |\psi_s|)$$
(4)

And:

$$\Psi_{s\alpha} = \sigma L_r I_{r\alpha} + \frac{M}{L_s} \Psi_s \tag{5}$$

$$\Psi_{s\beta} = \sigma L_r I_{r\beta} \tag{6}$$

$$\left|\overline{\Psi_{s}}\right| = \frac{\left|\overline{V_{s}}\right|}{w_{s}} \tag{7}$$

where,  $V_s$  is the stator voltage.

$$\sigma = 1 - \frac{M^2}{L_r L_s} \tag{8}$$

The rotor flux can be estimated by:

$$\Psi_{r\alpha} = \int_{0}^{t} (-R_{r} I_{r\alpha} + V_{r\alpha}) dt$$

$$\Psi_{r\beta} = \int_{0}^{t} (-R_{r} I_{r\beta} + V_{r\beta}) dt$$
(9)

And:

$$\psi_r = \sqrt{\Psi_{r\alpha}^2 + \Psi_{r\beta}^2} \tag{10}$$

The angle of rotor flux is calculated by:

$$\theta_r = \operatorname{arctg}(\frac{\Psi r\beta}{\Psi r\alpha}) \tag{11}$$

In twelve sectors DPC method a 2-level HC (see Figure 2) is used for the active power (Hp) and a two-level HC (see Figure 3) for the reactive power (Hq). Finally, based on the values of constants Hq and Hp and the position of the rotor flux (12 region command), the proposed switching table is as shown in Table 1.



Figure 2. Active power hysteresis comparator

 Table 1. Proposed switching table of twelve sectors DPC method

	Hq				
Ν	1		0		
	Нр				
	1	0	1	0	
1	1	6	3	5	
2	1	6	3	5	
3	2	1	4	6	
4	2	1	4	6	
5	3	2	5	1	
6	3	2	5	1	
7	4	3	6	2	
8	4	3	6	2	
9	5	4	1	3	
10	5	4	1	3	
11	6	5	2	4	
12	6	5	2	4	



Figure 3. Reactive power hysteresis comparator

# **3. TWELVE SECTORS DPC METHOD WITH NEURAL HYSTERESIS COMPARATORS**

In this section, The twelve sectors DPC method with neural hysteresis comparators (DPC-NHC) is a modification of the

conventional twelve sectors DPC method, where the two HCs, has been replaced by two neural controllers respectfully. This proposed method minimized the THD value of stator current, reactive/active power ripple compared to the conventional TSDPC method. The TSDPC method of the DFIG with the application of the NHC method is shown in Figure 4. This proposed method is easy to implement and simple method. However, the proposed neural controllers are the retropropagation of Levenberg-Marquardt (LM). The parameters of the LM algorithm is shown in Table 2. The structure of NHCs is illustrated in Figure 5. The block diagram of layer 1 and layer 2 is shown in Figure 6 and Figure 7 respectively.

The hidden layer of neural hysteresis comparator (NHC) is shown in Figure 8. Figure 9 shows the neural training performance of the neural networks algorithm for hysteresis comparators of reactive/active power.



Active and reactive power estimation

p{1}

Delays 1





Table 2. Parameters of the LM algorithm



netsum

tansig

a{1}

IW{1,1}



Figure 7. Layer 2

Figure 5. Block diagram of the neural hysteresis comparator



Figure 8. Hidden layer

## 4. RESULTS AND DISCUSSION

Simulations of the proposed strategies for a DFIG are conducted by using the Matlab/Simulink software. The proposed strategies will be tested and compared in two different configurations: robustness against parameter variations and reference tracking.

#### 4.1 Reference tracking test

In this section, the reactive/active power tracks almost perfectly their reference values (See Figures 13-14). On the other hand, the DPC-NHC strategy reduced the reactive and active power ripples compared to the conventional DPC strategy (See Figures 15-16).



Figure 9. Neural network training performance

Figures 10-11 show the THD of stator current for DPC-NHC and conventional DPC method one respectively. It can be clearly observed that the THD is minimized for the DPC-NHC method (THD = 0.74 %) when compared to conventional DPC (THD = 0.32%). It is clear from the results that the DPC-NHC has satisfied performance.





Figure 10. THD (DPC)



Figure 11. THD (DPC-NHC)



Figure 12. Active power (RTT)



**Figure 13.** Reactive power (RTT)



Figure 14. Zoom in the active power (RTT)



Figure 15. Zoom in the reactive power (RTT)

#### 4.2 Robustness test (RT)

In this section, the parameters have been intentionally changed such as the values of the inductances  $L_r$  and  $L_s$  are divided by 2 and the resistances  $R_r$  and  $R_s$  are multiplied by 2. The DPC-NHC method reduced the active and reactive power ripples compared to the TSDPC strategy (See Figures 20-21). On the other hand, the active and stator reactive power track almost perfectly their reference values (See Figures 18-19).



Figure 16. THD (DPC)

Figures 16-17 show the THD of the current of both techniques. It can be clearly observed that the THD is minimized for DPC-NHC strategy (THD = 0.59 %) when compared to conventional DPC (THD = 1.29%). It can be concluded that the twelve sectors DPC-NHC method is more robust than the TSDPC strategy.



Figure 17. THD (DPC-NHC)



**Figure 18.** Active power (RT)



Figure 19. Reactive power (RT)



Figure 20. Zoom in the active power (RT)



Figure 21. Zoom in the reactive power (RT)

#### 5. CONCLUSION

In this work, the twelve sectors DPC method with neural hysteresis comparators is presented and it is compared with the conventional DPC method. The simulation results obtained for the proposed strategy illustrate a considerable reduction in active/reactive power ripple. On the other hand, the proposed DPC method reduced the THD of current compared to the traditional twelve sectors DPC method.

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### APPENDIX

Table 3.	DFIG parameters	s [20, 21]
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Pn	1.5 MW	
Р	2	
Vn	380V	
Rs	$0.012\Omega$	
Lr	0.0136H	
Ls	0.0137H	
Rr	$0.021\Omega$	
Lm	0.0135H	
Fr	0.0024Nm.s/rad	
J	1000 Kg.m <sup>2</sup>	
f	50Hz	