directly correlated to the vorticity and pressure distribution around the blade. The effect of the LEV physical size on the total circulation over the suction surfaces explains the difference between rigid and flexible blades. Fig.11 (a) and (b) represent the variation of the mean power coefficient C_P and the input power required to deform the blades for the aforementioned cases. It can be seen that the higher C_P values are recorded at a0/c=0.2.

8. CONCLUSION

Blade shape for a VATT has a large effect on the turbine efficiency, which is primarily attributed to the nature of the interaction between the blade and the detached LEV vortex. The control and the manipulation of this expected interaction is the solution for an efficient model of VATT. As the turbine rotates, the blade can interact with the vortices generated by the blade itself or by previous blades. The ability of the blade to change its shape and therefore the flow structure interaction during the turbine rotation can produce significant improvements. The change in the blade camber line gives rise to a typical larger horizontal surface where the LEV is expected to act on. Moreover, this correction is able also to alter the flow angle of attacks and therefore the leading edge vortex time of formation, which results in an improved lift and power extraction. Computational results indicate that this strategy of control indeed enhance the VATT performance. For a tip speed ratio $\lambda=3.5$, a frequency zi=4, and a camber amplitude a0/c=0.2; the power coefficient (CP) rises about 20 % relative to the original turbine.

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