

Thermal expansion effect on thickness-shear vibrations in a piezoelectric quartz filter with dot-ring electrodes

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<https://doi.org/10.18280/ijht.360223>

Received: 27 September 2017

Accepted: 3 February 2018

Keywords:

quartz crystals, thickness-shear vibration, filter, thermal expansion effect

ABSTRACT

This paper aims to disclose the thermal expansion effect on thickness-shear vibrations of quartz filters. To this end, a brand-new “dot-ring” electrode structure was proposed for quartz filter operating in thickness-shear modes (TSMs). Then, a reasonable solution to the government equations of thermal expansion was derived, and the thermal expansion effect on the operation modes and vibration frequencies of the filter were examined in details. Through the rational design of electrode size and quartz plate thickness, a frequency interval was determined with two trapped modes. Under the working temperature between -55°C and 85°C , the electrode sizes changed with the thermal expansion; the resonance frequency declined with the increase of temperature. However, the frequency difference considering the thermal expansion effect is extremely small, indicating that the quartz crystal filter has good thermal stability. The research findings shed new light on the design of quartz filters.

1. INTRODUCTION

Piezoelectric crystals are the main raw materials of acoustic wave resonators, filters and sensors. For instance, AT-cut quartz crystals are often made into acoustic wave devices which operate in the thickness-shear mode (TSM) of a plate [1,2]. It is extremely difficult to simulate these materials with 3D theory of linear piezoelectricity, due to their high anisotropy and electromechanical coupling. A viable alternative is to develop approximate 2D plate equations, such as the single scalar differential equation for the fundamental and the overtone TSMs. This equation was derived for AT-cut quartz plates [3-6], and later applied to other anisotropic materials [7-9].

The traditional design of resonators contains square/rectangular dielectric and piezoelectric layers and square electrodes [9-11]. In crystal filters, however, two square electrodes are arranged above the piezoelectric crystals. The acoustic waves from the square electrodes propagate in all directions [12-13], leading to concentrated electric field, stress and temperature [14] in the electrode corners. In this case, the materials may deteriorate or even fail. Therefore, it is meaningful to consider the thermal expansion effect on thickness-shear vibrations. Nevertheless, there is little theoretical analysis on this effect of crystal filters, because the situation is too complicated to be explained clearly with 2D equations [15-20].

Considering the above, this paper proposes a brand-new “dot-ring” electrode structure for quartz filter. The corner-less design of the structure helps eliminate the concentration of electric field. Then, a theoretical analysis was performed to acquire the basic vibration features of the quartz filter with the proposed electrodes, and investigate the thermal expansion effect.

2. THERMAL EXPANSION

The research object is an AT-cut quartz plate filter. As shown in Figure 1, the plate is $2h$ in thickness and ρ in mass density. There is a thin, elliptical dot electrode in the central region and a ring electrode in the annular region atop the quartz plate. The two electrodes form the “dot-ring” structure. The mass density and thickness of both electrodes are denoted as ρ' and $2h'$, respectively. The semi-major axis of the elliptical electrode points to the x_1 direction, while the semi-minor axis of the elliptical electrode points to the x_3 direction. The two axes are respectively denoted as $a_i R_i$ and

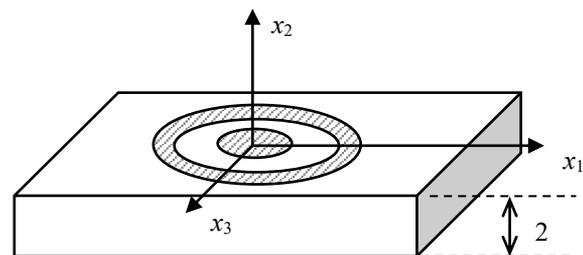


Figure 1. An FBAR filter with dot-ring driving electrodes

R_i , where $i=0, 1$ and 2 and the ratio a_i will be determined by the later formula.

The thermal expansion coefficient can be expressed as [21]:

$$\alpha = \Delta L / (L * \Delta T). \quad (1)$$

The electrode radius and the quartz plate thickness both change under thermal expansion. Considering the linear expansion coefficient of quartz crystal filter, the linear

expansion coefficient along axis x_2 is about half of the linear expansion coefficient vertical to axis x_2 . Table 1 lists the two

coefficients from -250 °C to 500 °C.

Table 1. The linear thermal expansion coefficients of the x_1 and x_2 axis

T (°C)	-250	-200	-100	0	100	200	300	400	500
$\alpha_1 \times 10^{-6}/(^{\circ}\text{C})$	8.60	9.90	11.92	13.24	14.45	15.61	16.89	18.5	20.91
$\alpha_2 \times 10^{-6}/(^{\circ}\text{C})$	4.10	5.50	6.08	7.10	7.79	8.75	9.60	10.65	12.22

The linear expansion coefficient at any angle φ relative to axis x_2 can be expressed as [21]:

$$\alpha_L = \alpha_2 + (\alpha_1 - \alpha_2) \sin^2 \varphi. \quad (2)$$

At room temperature, $\alpha_L = (7.48 + 6.23 \sin^2 \varphi) \times 10^{-6}$.

3. GOVERNING EQUATIONS

For time-harmonic motions of a filter at resonance frequency ω , all fields have the same time-dependence with a common factor $\exp(i\omega t)$. Thus, the TSM displacement of order n can be expressed as [3-6]:

$$u_1^n(x_1, x_2, x_3, t) = \sum_{n=1,3,5,\dots}^{\infty} u_1^n(x_1, x_3, t) \sin(\eta_n x_2). \quad (3)$$

If there is no top driving electrode, the in-plane variation $u_1^n(x_1, x_3)$ in the TSM mode of order n is governed by [3-6]:

$$M_n \frac{\partial^2 u_1^n}{\partial x_1^2} + c_{55} \frac{\partial^2 u_1^n}{\partial x_3^2} - \frac{n^2 \pi^2 \bar{c}_{66}}{4h^2} u_1^n = \rho \ddot{u}_1^n \quad (4)$$

If there is a driving electrode, the in-plane variation $u_1^n(x_1, x_3)$ in the TSM mode of order n is governed by:

$$M_n \frac{\partial^2 u_1^n}{\partial x_1^2} + c_{55} \frac{\partial^2 u_1^n}{\partial x_3^2} - \frac{n^2 \pi^2 \hat{c}_{66}}{4h^2} u_1^n = \rho \ddot{u}_1^n \quad (5)$$

In Eq(4) and Eq(5), c_{55} is the elastic constant of quartz crystals. The M_n can be determined by:

$$M_n = c_{11} + (c_{12} + c_{66})\gamma + \frac{4(\gamma \bar{c}_{66} - c_{66})(\gamma c_{22} + c_{12})}{c_{22} n \pi \kappa} \cot \frac{\kappa n \pi}{2}, \quad (6)$$

where c_{11} , c_{12} , c_{22} and c_{66} are the elastic constants of quartz crystals. The coefficients \bar{c}_{66} , \hat{c}_{66} , γ and κ can be obtained by:

$$\bar{c}_{66} = c_{66} + \frac{e_{26}^2}{\varepsilon_{22}}, \quad \kappa = \left(\frac{\bar{c}_{66}}{c_{22}} \right)^{1/2}, \quad \gamma = \frac{c_{12} + c_{66}}{\bar{c}_{66} - c_{22}}, \quad (7)$$

$$\hat{c}_{66} = \bar{c}_{66} \left(1 - \frac{8\bar{k}_{26}^2}{n^2 \pi^2} - 2R' \right), \quad (8)$$

where e_{26} and ε_{22} are the piezoelectric constants and dielectric constants of quartz crystals, respectively. These constants can be determined by:

$$\bar{k}_{26}^2 = \frac{e_{26}^2}{\bar{c}_{66} \varepsilon_{22}}, \quad R' = \frac{2\rho' h'}{\rho h}. \quad (9)$$

In the (x_1, x_3) plane, the elliptical electrode can be described as:

$$\frac{x_1^2}{R_i^2 M_n / c_{55}} + \frac{x_3^2}{R_i^2} = 1, \quad i = 0, 1, 2. \quad (10)$$

The semi-major and semi-minor axes are $\sqrt{M_n / c_{55}} R_i$ and R_i , respectively. Then, a new coordinate system (λ_1, λ_3) was introduced as:

$$x_1 = \lambda_1 \sqrt{M_n / c_{55}}, \quad x_3 = \lambda_3. \quad (11)$$

The ellipses in Eq(10) can be converted into circle equations:

$$\frac{\lambda_1^2}{R_i^2} + \frac{\lambda_3^2}{R_i^2} = 1, \quad i = 0, 1, 2. \quad (12)$$

Then, the polar coordinates were introduced: let dependence θ of the fields be $\cos(m\theta)$ where $m=0, 1, 2, \dots$. Thus, Eq(5) and Eq(4) can be rewritten as:

$$\begin{aligned} \frac{\partial^2 u_1^n(r)}{\partial r^2} + \frac{1}{r} \frac{\partial u_1^n(r)}{\partial r} - \frac{m^2}{r^2} u_1^n(r) + \rho c_{55}^{-1} (\omega^2 - \hat{\omega}_\infty^2) u_1^n(r) &= 0, \\ \frac{\partial^2 u_1^n(r)}{\partial r^2} + \frac{1}{r} \frac{\partial u_1^n(r)}{\partial r} - \frac{m^2}{r^2} u_1^n(r) - \rho c_{55}^{-1} (\bar{\omega}_\infty^2 - \omega^2) u_1^n(r) &= 0, \end{aligned} \quad (13)$$

where $\hat{\omega}_\infty$ and $\bar{\omega}_\infty$ are the unbounded plate TSM resonant frequencies for plates with or without electrode, respectively. The two parameters obey $\bar{\omega}_\infty > \hat{\omega}_\infty$ because the resonant frequencies are dragged down by electrode inertia. The $\hat{\omega}_\infty$ and $\bar{\omega}_\infty$ can be described as:

$$\hat{\omega}_\infty^2 = \frac{n^2 \pi^2 \hat{c}_{66}}{4\rho h^2}, \quad \bar{\omega}_\infty^2 = \frac{n^2 \pi^2 \bar{c}_{66}}{4\rho h^2}. \quad (14)$$

For ‘‘trapped modes’’, the vibration gradually attenuates away from an electrode edge, especially when r approaches infinity. The boundary conditions are:

$$\begin{aligned} u_1^n &\text{ is finite, } r = 0, \\ u_1^n &\rightarrow 0, \quad r \rightarrow \infty. \end{aligned} \quad (15)$$

4. ANALYTICAL SOLUTION

The following conditions are required to solve Eq(13):

$$\begin{aligned} \beta_1^2 &= \rho c_{55}^{-1}(\omega^2 - \hat{\omega}_\infty^2) > 0, \\ \beta_2^2 &= \rho c_{55}^{-1}(\bar{\omega}_\infty^2 - \omega^2) > 0. \end{aligned} \quad (16)$$

The above equation defines a frequency interval for the trapped modes of interest: $\hat{\omega}_\infty < \omega < \bar{\omega}_\infty$. Based on the separate variables in polar coordinates, we have:

$$\begin{aligned} \xi_1 &= \beta_1 r, \quad r < R_0 \text{ and } R_1 < r < R_2, \\ \xi_2 &= \beta_2 r, \quad R_0 < r < R_1 \text{ and } R_2 < r < \infty. \end{aligned} \quad (17)$$

Then, Eq(13) can be converted into:

$$\begin{aligned} \frac{\partial^2 u_1^n(\xi_1)}{\partial \xi_1^2} + \frac{1}{\xi_1} \frac{\partial u_1^n(\xi_1)}{\partial \xi_1} + \left(1 - \frac{m^2}{\xi_1^2}\right) u_1^n(\xi_1) &= 0, \\ 0 < r < R_0 \text{ and } R_1 < r < R_2, \\ \frac{\partial^2 u_1^n(\xi_2)}{\partial \xi_2^2} + \frac{1}{\xi_2} \frac{\partial u_1^n(\xi_2)}{\partial \xi_2} - \left(1 + \frac{m^2}{\xi_2^2}\right) u_1^n(\xi_2) &= 0, \\ R_0 < r < R_1 \text{ and } R_2 < r < \infty. \end{aligned} \quad (18)$$

The two sub-equations of Eq(18) are the Bessel function and modified Bessel function of order m , respectively. Then, the general solution to Eq(18) satisfying Eq(15) can be written as:

$$\begin{aligned} u_1^n(r, \theta) &= A_1 J_m(\beta_1 r) \cos(m\theta), & 0 < r < R_0, \\ u_1^n(r, \theta) &= (A_2 I_m(\beta_2 r) + A_3 K_m(\beta_2 r)) \cos(m\theta), & R_0 < r < R_1, \\ u_1^n(r, \theta) &= (A_4 J_m(\beta_1 r) + A_5 Y_m(\beta_1 r)) \cos(m\theta), & R_1 < r < R_2, \\ u_1^n(r, \theta) &= A_6 K_m(\beta_2 r) \cos(m\theta), & R_2 < r < \infty, \end{aligned} \quad (19)$$

where $A_1 \sim A_6$ are unknown constants; J_m and Y_m are the m th-order Bessel functions of the first kind and second kind; I_m and K_m are the m th-order modified Bessel functions of the first kind and second kind. The solution to Eq(19) must satisfy the following continuous conditions:

$$\begin{aligned} u_1^n(R_0^-) &= u_1^n(R_0^+), \quad \frac{du_1^n}{dr} \Big|_{R_0^-} = \frac{du_1^n}{dr} \Big|_{R_0^+}, \\ u_1^n(R_1^-) &= u_1^n(R_1^+), \quad \frac{du_1^n}{dr} \Big|_{R_1^-} = \frac{du_1^n}{dr} \Big|_{R_1^+}, \\ u_1^n(R_2^-) &= u_1^n(R_2^+), \quad \frac{du_1^n}{dr} \Big|_{R_2^-} = \frac{du_1^n}{dr} \Big|_{R_2^+}. \end{aligned} \quad (20)$$

Substituting Eq(19) into Eq(20), we have six linear homogeneous equations for $A_1 \sim A_6$. For nontrivial solutions, the determinant of the coefficient matrix should be eliminated, producing the frequency equation. The modes can be determined by the corresponding nontrivial solutions of $A_1 \sim A_6$. The numerical solutions are obtained with Matlab by selecting appropriate parameters.

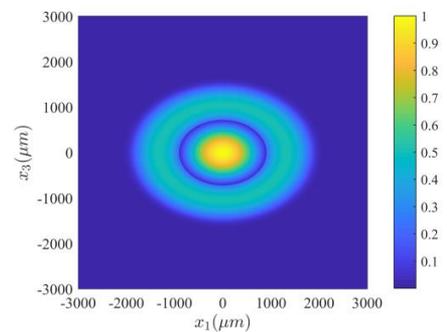
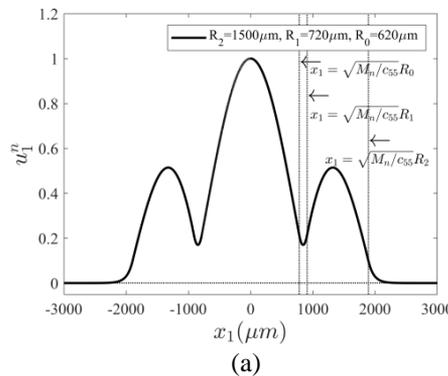
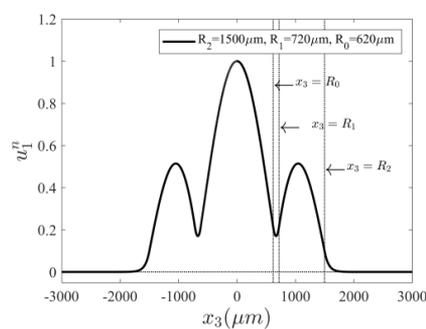
5. NUMERICAL SIMULATION AND RESULTS ANALYSIS

The numerical example is a filter operating at the fundamental TSMs. For the remainder of this paper, the

values of n and m are fixed as $n=1$ and $m=0$. The other parameters are as follows: electrode-plate mass ratio $R'=0.1$, plate thickness $2h=200 \mu\text{m}$, electrodes radii $R_0=620 \mu\text{m}$, $R_1=720 \mu\text{m}$ and $R_2=1,500 \mu\text{m}$. The trapped modes are the interest modes and found in the narrow frequency interval determined by Eq(14). By this equation, it is determined that $\hat{\omega}_\infty = 4.6492 \times 10^7 \text{ rad/s}$ and $\bar{\omega}_\infty = 5.2185 \times 10^7 \text{ rad/s}$. The two trapped modes of interest were found in the frequency interval $(\hat{\omega}_\infty, \bar{\omega}_\infty)$: $\omega_I = 4.9361 \times 10^7 \text{ rad/s}$ and $\omega_{II} = 4.9917 \times 10^7 \text{ rad/s}$, in this case.

Table 2. Numerical value of electrode radius and plate thickness at different temperatures

$T(^{\circ}\text{C})$	$R_0(\mu\text{m})$	$R_1(\mu\text{m})$	$R_2(\mu\text{m})$	$h(\mu\text{m})$
-55	619.35	719.25	1,498.44	99.95
-35	619.51	719.43	1,498.82	99.96
-15	619.67	719.62	1,499.20	99.97
5	619.83	719.81	1,499.60	99.99
25	620	720	1,500	100
45	620.17	720.20	1,500.41	100.01
65	620.34	720.40	1,500.83	100.03
85	620.52	720.60	1,501.25	100.04



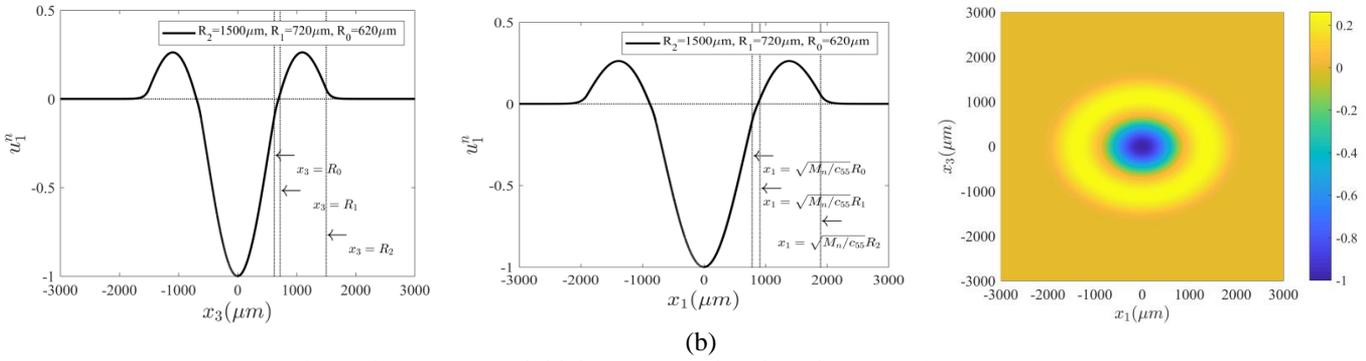


Figure 2. Two trapped thickness-extensional modes in the frequency interval

The two trapped modes bear high resemblance with each other, with a weak dependence on the in-plane mode variation. Figure 2 illustrates the cross-section of the two modes along $x_1=0$ and $x_3=0$. The mode in Figure 2(a) has no nodal line (point) except at the edges, but there exists a gap between the ring and dot electrodes. The mode vibrated under the dot electrode, attenuated between the ring and dot electrodes, and vibrated again under the ring electrode. The thickness-shear strain was always positive thanks to the thickness-shear displacement with $n=1$. The mode in Figure 2(b) has one nodal line between the ring and dot electrodes. The two sides of that nodal line vibrated in opposite directions. However, the charge of the electrode system is not cancelled out.

For better view, the contours of the two modes are also presented in Figure 2. It can be seen that the electrodes are oval in shape, and the semi-major axis ($\sqrt{M_{11}/c_{55}}R_i$) and semi-minor axis (R_i) are along axes x_1 and x_3 , respectively. The ratio between them was 1.47, which is very close to the optimal electrode shape in References [22-24].

In the numerical simulation, the working temperature of the filter was set to $-55^\circ\text{C} \sim 85^\circ\text{C}$. The separate points in Table 2 were fitted to obtain the thermal expansion curve in the temperature range. Then, the thermal expansion coefficients in the range were integrated to acquire the numerical value of each length at the corresponding varied more violently than the plate thickness with the temperature. Since a_1 is about half of a_2 , the electrode size varied more violently than the plate thickness with the same temperature change. Based on these values, $\hat{\omega}_\infty$ and $\bar{\omega}_\infty$ were calculated by Eq(14). In each case, the two trapped modes of interest were found in the frequency interval.

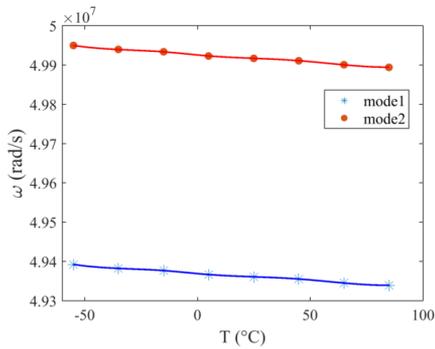


Figure 3. The frequency of trapped modes varies with temperature.

Figure 3 presents two frequency-temperature curves. The first and second modes are respectively expressed with the star

line and the point line. In the first mode, the filter could operate with the in-phase vibration of the whole plate; In the second mode, the filter could also operate with the out-of-phase vibration of the dot and ring electrodes. It is clear that the temperature is negatively correlated with resonance frequency; both plate thickness and electrode size increased with the temperature. Thus, there is a negative correlation between plate thickness/electrode size and resonance frequency.

As shown in Figure 3, the frequencies varied little with temperatures. In mode 1, the maximum and minimum frequencies were $49.3926 \times 10^6 \text{ rad/s}$ and $49.3395 \times 10^6 \text{ rad/s}$, respectively. This means the quartz crystal filter has good thermal stability.

Figure 4 show the effects of temperature on the operation modes. All parameters are the same as those in Figure 2, except that plate thickness and electrode size are variants. The figure reveals no obvious impact of temperature (T) on mode shapes. This is particularly true for mode one: the three temperature curves at -55°C , 25°C and 85°C almost coincided completely. For mode two, there was a significant difference between the vibration modes in the ring electrode region.

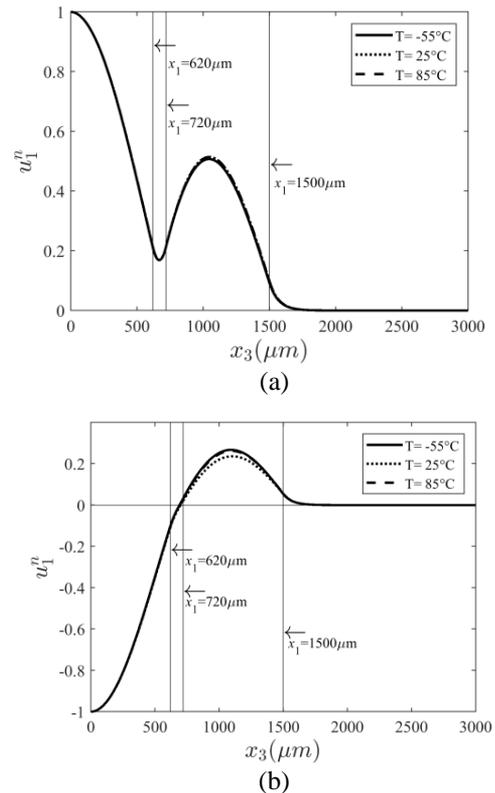


Figure 4. Effects of the temperatures T on the operating modes

The electrode scale is crucial to filter design. To disclose the effect of electrode scale, three kinds of electrode scales were designed and compared with each other. The shapes of the trapped modes are recorded in Figure 5. In the remainder of this paper, the value of R_2 is fixed as $R_2=1,500\ \mu\text{m}$, while the values of other parameters are specified in individual figures. As shown in Figure 5, the radii R_0 and R_1 were time-varying, resulting in changes to the area of the dot or ring electrode region. With the increase of R_0 , the vibration under the ring electrode grew weaker but remained basically the same under

the dot electrode. This is because the electrode scale is positively correlated with the vibration amplitude. As R_0 grew longer, the annular region shrank in size and became comparable to the central region. Thus, the vibration under the annular region attenuated. With the increase of R_1 , the vibration became weaker under the ring electrode, the annular region got smaller, the distance grew wider. A possible reason lies in the weak interaction between the two electrodes when the distance was wide.

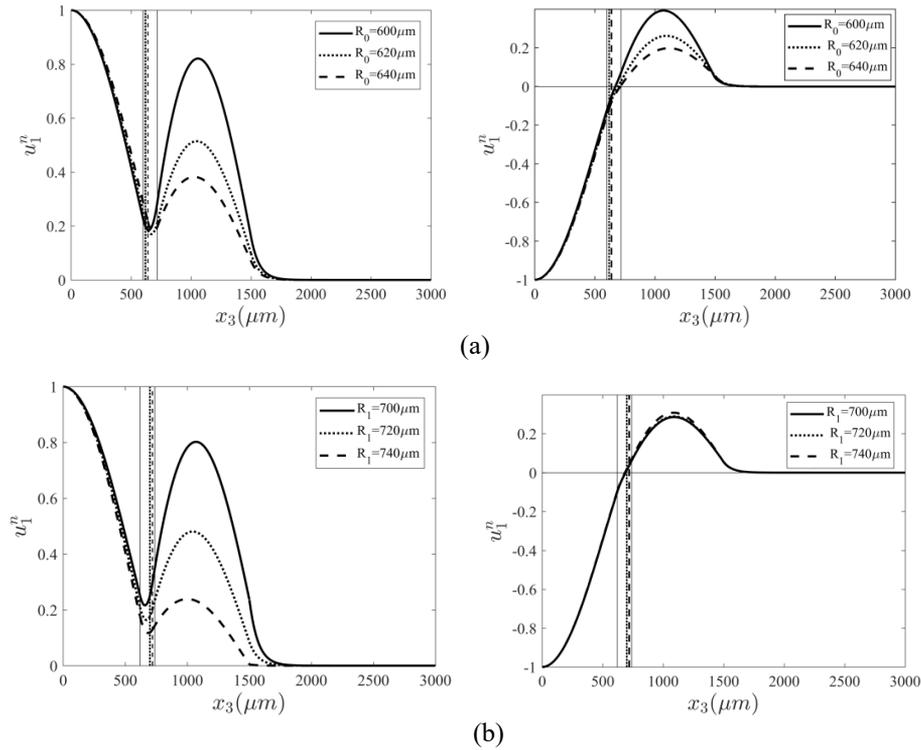


Figure 5. Effects of the radius of the electrode R_0 and R_1 on the operating modes.

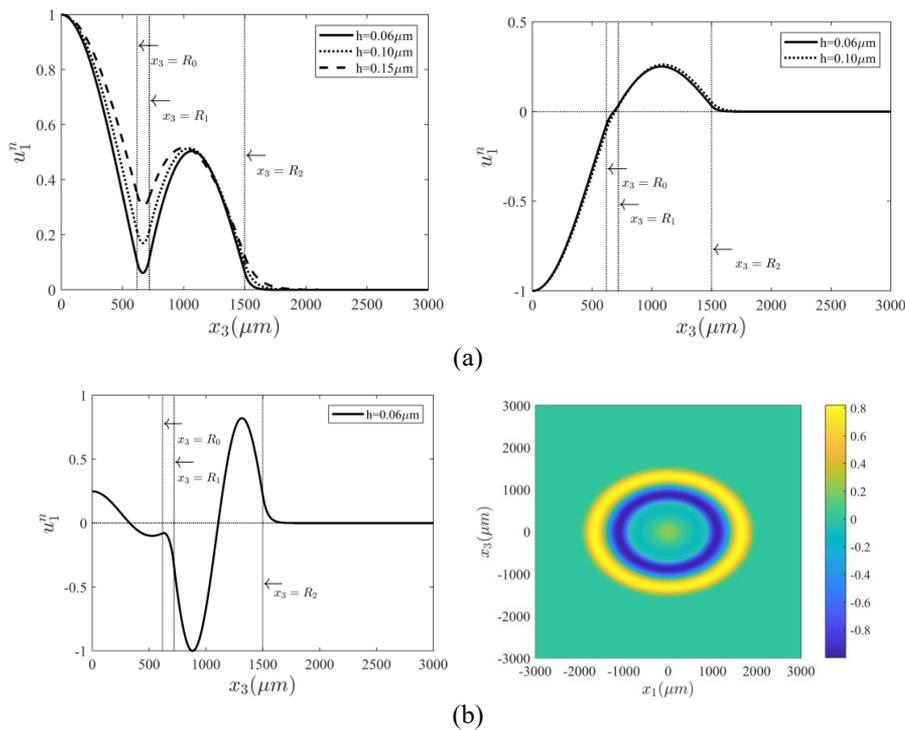


Figure 6. Effects of the half quartz plate thickness h on the operating modes

Table 3. Average and difference of the frequencies of two operating modes at different temperatures.

$T(^{\circ}\text{C})$	$\omega_1(\text{rad/s})$	$\omega_2(\text{rad/s})$	$(f_1+f_2)/2(\text{MHz})$	f_2-f_1 (kHz)
-55	49,392,632.14	49,949,972.75	7.905,4	88.703,5
-35	49,382,480.51	49,939,629.50	7.903,8	88.673,0
-15	49,376,940.6	49,933,658.95	7.902,9	88.604,5
5	49,366,806.56	49,923,271.81	7.901,3	88.564,2
25	49,361,115.00	49,917,211.46	7.900,3	88.505,5
45	49,355,475.27	49,911,129.47	7.899,4	88.435,1
65	49,345,284.49	49,900,661.59	7.897,7	88.391,0
85	49,339,532.84	49,894,517.40	7.896,8	88.328,5

Table 4. Average and difference of the frequencies of two operating modes with different dimensions.

$R_o(\mu\text{m})$	$R_i(\mu\text{m})$	$h(\mu\text{m})$	$\omega_1(\text{rad/s})$	$\omega_2(\text{rad/s})$	$(f_1+f_2)/2(\text{MHz})$	f_2-f_1 (kHz)
620	720	100	49,361,115.00	49,917,211.46	7.900,3	88.505,5
600	720	100	49,479,635.10	50,029,419.08	7.918,7	87.500,8
640	720	100	49,172,948.28	49,863,881.04	7.881,1	109.965,3
620	700	100	49,164,215.46	49,914,289.84	7.884,4	119.378,0
620	740	100	49,524,037.54	49,933,262.10	7.914,6	65.1301,1
630	710	100	49,174,701.48	49,880,317.05	7.882,5	112.302,2
610	730	100	49,512,410.12	49,967,633.45	7.916,4	72.451,0
620	720	60	79,589,986.47	79,691,441.38	12.675,2	16.147,1
620	720	150	34,281,745.84	--	--	--

Figure 6 presents the effects of h on the operation modes of the filter. All parameters are the same as those in Figure 2, except that plate thickness is a variant. It is observed that both modes and the number of frequency roots were sensitive to the plate thickness. Under $h=0.06$ m, three trapped modes were discovered in the frequency interval. For better view, the contour of the third mode is also displayed in Figure 6. This mode contains two nodal lines: one in the dot electrode region and the other in the ring electrode region. Thus, the third mode cannot cancel out the charge in the electrode region and is not an ideal operation mode.

Our filter design adopts the average and difference of the first and second frequency roots, instead of the frequencies. When the frequencies of the two modes are close enough and their resonance peaks overlap to a certain degree, the two modes can be used together as a filter with twice the bandwidth. Tables 3-4 list the frequencies of the modes in Figures 2-6.

The frequency difference is related to the band pass width of the filter. As shown in Table 3, the average of the first and second frequency roots was close to 7.9 MHz; the frequency difference amounts to hundreds of Hz. As shown in Table 4, the frequency difference amounts to tens of thousands of Hz, much larger than the frequency difference in Table 3. Therefore, the thermal expansion effect on the frequency difference can be neglected in filter operation, and the accuracy of frequency should reach kHz.

6. CONCLUSIONS

This paper proposes a novel “dot-ring” electrode structure for quartz filter. The corner-less design of the structure helps eliminate the concentration of electric field. Then, a theoretical analysis was performed to acquire the basic vibration features of the quartz filter with the proposed electrodes, and investigate the thermal expansion effect.

The simulation confirms the importance of the electrode size and quartz plate thickness in the design of filters. The proper design can reveal some trapped modes, whose vibrations are covered by the dot-ring electrodes. The trapped

modes are the ideal operation mode, with a nodal line in the gap between the ring and the dot electrodes. Both the location of the nodal line and the field attenuation rate are sensitive to the geometric and physical parameters of the electrodes and plate. Under the working temperature between -55 °C and 85 °C, the electrode sizes changed with the thermal expansion; the resonance frequency declined with the increase of temperature. However, the frequency difference considering the thermal expansion effect is extremely small, indicating that the quartz crystal filter has good thermal stability.

ACKNOWLEDGMENT

This research was supported by the Ningbo Natural Science Foundation in Zhejiang province, China under Grant No. 2017A610105, and the Public Projects of Zhejiang Province (No. 2015C31150).

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NOMENCLATURE

x	cartesian coordinates, m
h	height, m
R	semi-minor axis, m
a	dimensionless ratio of semi-major axis/ semi-minor axis
L	length, m
T	temperature, K
u	dimensionless displacement
n	vibration order
M	coefficient of equation, N/m^2
c	elastic coefficient, N/m^2
R'	dimensionless electrode-plate mass ratio
f	frequency, Hz
m	mode order
r	polar coordinates, m
θ	polar coordinates, rad

Greek symbols

α	thermal expansion coefficient, K^{-1}
λ	coordinates, m
ρ	density, $kg.m^{-3}$
φ	angle relative to axis x_2 , rad
η	wave number, m^{-1}
γ	dimensionless ratio of elastic coefficients
ω	circular frequency, $rad.s^{-1}$
β	intermediate parameters
ζ	intermediate parameters

Subscripts

∞	infinite plate
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