

## A New Harris Hawks-Cuckoo Search Optimizer for Multilevel Thresholding of Thermogram Images

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#### ABSTRACT

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#### Keywords:

optimizer, Harris Hawks optimization, cuckoo search, multilevel thresholding, thermogram image analysis The exploitation capability of the Harris Hawks optimization (HHO) is limited. This problem is solved here by incorporating features of Cuckoo search (CS). This paper proposes a new algorithm called Harris hawks-cuckoo search (HHO-CS) algorithm. The algorithm is validated using 23 Benchmark functions. A statistical analysis is carried out. Convergence of the proposed algorithm is studied. Nonetheless, converting color breast thermogram images into grayscale for segmentation is not effective. To overcome the problem, we suggest an RGB colour component based multilevel thresholding method for breast cancer thermogram image analysis. Here, 8 different images from the Database for Research Mastology with Infrared images are considered for the experiments. Both 1D Otsu's between-class variance and Kapur's entropy are considered for a fair comparison. Our proposal is evaluated using the performance metrics - Peak Signal to Noise Ratio (PSNR), Feature Similarity Index (FSIM), Structure Similarity Index (SSIM). The suggested method outperforms the grayscale based multilevel thresholding method proposed earlier. Moreover, our method using 1D Otsu's fitness functions performs better than Kapur's entropy based approach. The proposal would be useful for analysis of infrared images. Finally, the proposed HHO-CS algorithm may be useful for function optimization to solve real world engineering problems.

#### **1. INTRODUCTION**

Breast cancer is most common among women. Over 2.1 million women get affected each year, and the death rates are highly related to the breast cancer [1]. It is the second most common cancer in women after lungs cancer. Breast Cancer mostly begins in the ducts or lobules after uncontrolled growth of the cells. Breast cancer can spread to distant organs, so an early treatment is required. Cancer is a disease with multiple factors, so advanced screening of the breasts is required for analysis of the tumor formation. Breast cancer can be classified in several stages, the initial stage, which is known as DCIS (ductal carcinoma in situ), the growth of cells is limited in ducts. In the next stage, the formation of tumor occurs, and also has a small group of cancer cells. When the size of the tumor grows, it spreads to lymph nodes and distant organs such as bones, liver, brain or lungs.

Advanced screening of breasts is required for analysis of tumor formation as an extra aid to a radio-physicist. There are various Medical imaging techniques used for early analysis of breast cancer, Such as Breast Ultrasound (Sonogram), Magnetic Resonance (MRI), Thermography, Mammography, Positron Emission Tomography (PET), Computed Tomography (CT), Integrated PET/CT, MRI and PET, Ultrasound and MRI.

Mammography is one of the popular diagnostic techniques used for the detection of breast cancer. Mammography involves exposure to X-ray radiation on the human body. Due to the exposure to radiation, there is a possibility of further cancer cell growth. Sometimes Mammography, Breast MRI and Breast Ultrasound show "false-positive" results, in which the person needs an additional test or even more. This could lead to another mammogram or a different test.

On the other hand, thermography is a clinical procedure where a thermal camera captures the infrared radiation of the human body at controlled room temperature and produces the digital thermal images. A body emits infrared radiation above absolute zero temperature. A thermal image shows the temperature variations of the body. The infrared radiation emitted by the surface of the body has wavelength ranges from  $0.8\mu$ m to  $10 \ \mu$ m. Thermography is a non-invasive process, no exposure to radiations and does not involve in compression of breast tissues [2]. Thermography provides information on the growth of cancer cells before the formation of a tumour. No radiation is involved as the temperature variation of the body provides vascular activity information.

Image Segmentation Partitions images into regions into homogeneous classes. For image segmentation, several techniques have been studied throughout the years. Multilevel thresholding is the easiest method in image segmentation. In color images, multilevel thresholding partitions, images into different classes based on threshold levels of each R, G, B histogram components. The thresholding based segmentation method is divided into parametric and non-parametric. Note that the parametric method calculates the probability density function of each class, whereas the nonparametric measure class variance, entropy to get the optimal threshold values [3]. Due to the computational complexity of the parametric approach, nonparametric methods are used. Various optimization techniques are used in multilevel thresholding using nonparametric approaches to get the best threshold values. Segmentation of medical images is popular in recent years as it is helpful for analysis of a particular part of the body.

In this work, a new optimization technique called Harris Hawks-Cuckoo Search (HHO-CS) is investigated. The Harris Hawks optimizer is found more popular for function optimization. However, its exploitation capability is limited, thereby not yielding to optimal or near optimal solutions. This has motivated us to incorporate the exploitation capability of the cuckoo search strategy. This is the real motivation behind the investigation of the proposed HHO-CS algorithm. Two different objective functions are used for a comparison. The suggested algorithm is used to obtain the optimal threshold values to segment colour thermogram images. The effectiveness of HHO-CS algorithm is validated with a set of 23 Benchmark functions and compared with Harris Hawks optimization [4] and Cuckoo Search algorithm [5]. For multilevel thresholding of thermogram images, experiments are performed based on Otsu's between-class variance and Kapur's entropy as the fitness functions. Our proposed HHO-CS technique is evaluated based on the performance metrics peak signal to noise ratio (PSNR), Feature similarity index (FSIM), Structure Similarity Index (SSIM). Results of objective function values, threshold levels of RGB component are also evaluated.

Converting colour thermal images into grayscale images makes it a difficult task to extract features due to poor contrast, low visual perception. Therefore, it is necessary to perform full colour image processing of the clinical images for research support. For the past few years, many optimization techniques are used to perform segmentation to get better quality segmented images. This has motivated us to investigate a method to segment colour thermogram images. Results are presented using 1D Otsu's objective function and Kapur's entropy.

Organization of the paper is as follows: Section 2 discusses the related work. The proposed HHO-CS algorithm is presented in Section 3. The methodology is discussed in Section 4. Results are presented in Section 5. Conclusions are given in Section 6.

#### 2. RELATED WORK

Díaz-Cortés et al. [6] in 2018 presented multilevel thresholding of Breast Thermal images using Dragonfly algorithm. The Segmentation of grayscale breast thermal images is performed by using the energy curve of images as an input. The colour Segmentation of satellite images using nature-inspired optimization algorithms are proposed by Bhandari et al. [7]. The performance of the algorithms was performed based on Otsu's between-class variance and Kapur's entropy as the objective functions. The Kapur's entropy based objective function has better performance and the Cuckoo search algorithm was found to be more efficient for Colour segmentation of satellite images.

He and Huang [8] presented an efficient krill herd (EKH) optimization technique for multilevel thresholding of colour images using Otsu's method, Kapur and Tsallis entropy as the objective functions. The efficient krill herd (EKH) algorithm shows better performance as compared to the krill herd algorithm (KH). Electro-magnetism optimization (EMO)

algorithm based multilevel thresholding is presented by Oliva et al. [9]. The Otsu's and Kapur's entropy criterion used as objective functions and the histogram of images are taken as the input. Oliva et al. [3] presented a hybrid Artificial Bee colony-Salp Swarm algorithm (ABC-SSA), for image segmentation. The hybrid approach performs better than ABC, SCA, SSO, SSA algorithms in a multilevel thresholding problem using Kapur's entropy as the objective function. Multilevel thresholding of Satellite images proposed by Pare et al. [10] using optimization techniques WDO, BFO, FA, ABC, DE and PSO by taking energy curves of image as an input. The objective functions based on Kapur's entropy, Tsallis entropy and Otsu's method are used. The Kapur's entropy based DE techniques produces better segmented images.

Multilevel thresholding using WDO and CS was proposed by Bhandari et al. [11] using Kapur's entropy as the objective function. Multilevel thresholding using various Optimization techniques are reported in the studies [12-15]. Horng et al. [16] presented multilevel thresholding based on honey bee mating optimization using the cross entropy as the objective function. Bhandari et al. [17] proposed a modified artificial Bee colony (MABC) optimizer for multilevel thresholding of satellite images through maximization of Otsu's between-class variance, Kapur's and Tsallis entropy. The MABC algorithm produces better segmented images as compared to ABC method.

#### 2.1 Harris Hawks Optimization

A nature-inspired Optimization algorithm called "Harris-Hawks optimization" algorithm was proposed by Heidari et al. in 2019. The Harris-hawks optimization technique is inspired by the hunting strategy of Harris-hawks and escaping of prey. The Harris-hawks catch prey by a "Surprise Pounce" or also known as "Seven kills" strategy. The Harris-hawks optimization technique also features exploration and exploitation phase [4].

#### 2.1.1 Exploration phase

The exploration phase of HHO algorithm consists of two strategies to detect the prey (Rabbit) by perching randomly on some locations, taking an equal chance q (in each perching plan), the perch based on the position of other hawks. The location of the rabbit is known as  $X_{rabbit}$ . The rabbit location for the condition q < 0.5 described in Eq. (1). When  $q \ge 0.5$ , hawks roost on random high trees inside their range of location.

$$X(t+1) = \begin{cases} X_{rand} - r_1 \mid X_{rand}(t) - 2r_2 X(t) \mid, q \ge 0.5\\ (X_{rabbit}(t) - X_m(t)) - r_3(LB + r_4(UB - LB)), q < 0.5 \end{cases}$$
(1)

where, The term X(t+1) represents updated position of Hawks in each iteration,  $X_{rabbit}(t)$  is the postion of rabbit,  $X_{rand}(t)$ is the position of Hawks chosen randomly, LB is the lower bound, UB is the upper bound, and  $X_m(t)$  is the average position of hawks. Random numbers  $r_1, r_2, r_3, r_4$  are used to explore different regions of Search space for the Hawks. The equation for the average position of hawks is given by:

$$X_{m}(t) = \frac{1}{N} \sum_{i=1}^{N} X_{i}(t)$$
(2)

where, X<sub>i</sub>(t) and N represents the location of each Hawk in

iteration *t* and number of Hawks, respectively. The transition from the Exploration Phase to Exploitation Phase occurs depending on the Perching strategy of Hawks on escaping prey (Rabbit). The initial energy  $E_0$  The value ranges from -1 to 1 for every iteration t. When the value of  $E_0$  decreases from 0 to -1, it signifies a weakening of the prey. In case the value of  $E_0$ increases from 0 to 1, it signifies strengthening of the prey. The escaping energy of the Prey also a key factor in the transition, which is modelled as:

$$E = 2E_0(1 - \frac{t}{T}) \tag{3}$$

2.1.2 Exploitation phase

The Hawks perform the "Surprise Pounce" strategy to catch the prey. There is also an escaping factor 'r' of the prey, where the value of r is greater than 0.5 signify higher chance of escape and less than or equal to 0 signify lower chance of escape of the rabbit. There are different phases of exploitation of prey based on the escaping factor and energy of the prey. The exploitation phases are shown in Figure 1.

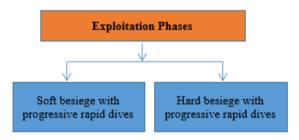


Figure 1. Exploitation phases of HHO

a. Soft Besiege

The Hawks perform Soft Besiege based on Rabbit's energy. The position of hawks for soft Besiege models as below.

$$X(t+1) = \Delta X(t) - E/JX_{rabbit}(t) - X(t)/$$
(4)

$$\Delta X(t) = X_{rabbit}(t) - X(t)$$
(5)

where, "J" is known as "Jump strength" of the Rabbit.

#### b. Hard Besiege

When the Rabbit is fagging, the hawks perform "Surprise Pounce" tactics, when the escaping factor value "r" is greater than or equal to 0.5 and the escaping energy is less than 0.5. For each iteration, the positions of hawks are updated using the equation.

$$X(t+1) = X_{rabbit}(t) - E \left| \Delta X(t) \right|$$
(6)

where, E is the energy.

c. Soft Besiege with progressive rapid dives

In Case of Escaping energy greater than or equal to 0.5 and the escaping factor less than 0.5 of the rabbit, the hawks perform soft besiege with progressive rapid dives. In this condition, the rabbit has sufficient energy to outflow). The Levy flight movement of Hawks depends on the zig-zag motion of the rabbit [6]. The Hawks update their position concerning the movements of the rabbit. The equations for this strategy can be described as below

$$Y = X_{rabbit}(t) - E \mid JX_{rabbit}(t) - X(t) \mid$$
(7)

$$Z = Y + S \times LF(D) \tag{8}$$

$$LF(x) = 0.01 \times \frac{u \times \sigma}{|v|^{\frac{1}{\beta}}}$$
(9)

where,

$$\sigma = \left(\frac{\Gamma(1+\beta) \times \sin(\frac{\pi\beta}{2})}{\Gamma(\frac{1+\beta}{2}) \times \beta \times 2^{(\frac{\beta-1}{2})}}\right)^{\frac{1}{\beta}}$$
(10)  
$$X(t+1) = \begin{cases} Y, F(Y) < F(X(t)) \\ Z, F(Y) < F(X(t)) \end{cases}$$

Note that LF is the Levy flight.

d. Hard Besiege with progressive rapid dives

When Escaping energy is less than 0.5 and escaping factor is less than 0.5, the rabbit is completely exhausted and has lowlevel energy, the Hawks perform hard besiege with rapid dives to catch the rabbit. In this stage, the hawks successfully catch the rabbit. The Levy flight method is also used in this phase. The equation for the position of hawks, for each iteration, is given below:

$$X(t+1) = \begin{cases} Y, & if \ F(Y) < F(X(t)) \\ Z, & if \ F(Z) < F(X(t)) \end{cases}$$
(11)

$$Y = X_{rabbit}(t) - E/JX_{rabbit}(t) - X_m(t)$$
(12)

$$Z = Y + S \times LF(D) \tag{13}$$

#### 2.2 Cuckoo search optimization

Nature-inspired Cuckoo Search optimization was proposed by Yang and Deb in 2009 [5]. The Cuckoo Search algorithm is based on the brooding parasitism of Cuckoo birds as they use another host bird's nest for breeding. The phases of the cuckoo search algorithm are described below

1) A cuckoo bird lays one egg at a time and pass down to another bird's nest;

2) The best nests with good quality eggs are carried over to the next generations;

3) The number of host nests is fixed, and the host bird can discover an egg with a probability of  $p_a \in [0,1]$ . Interestingly, the host bird can either throw the egg or abandon the nest immediately. The number of nests "*n*" and " $p_a$ " are replaced with new solutions.

The mathematical equation, for each iteration, is modelled as below.

$$x_i^{(t+1)} = x_i^{(t)} + \alpha \oplus L \acute{e}vy (\lambda)$$
(14)

the equation for the levy flight mechanism is given below.

$$L\acute{e}vy \sim u = t^{-\lambda}, (1 < \lambda \le 3)$$
(15)

where, 'u' is the variable and ' $\lambda$ ' is a constant.

### 3. PROPOSED HARRIS HAWKS-CUCKOO SEARCH OPTIMIZER

Harris Hawks Optimization technique performs good exploration tactics to catch the prey to reach a global best solution, whereas the weak exploitation capability of hawks signifies a higher chance of getting into local optima. To enhance the performance of HHO, the exploitation capability of Cuckoo search mechanism is inherited here. The location of hawks is updated by:

$$\begin{aligned} X(t+1) &= \\ \begin{cases} X_{rand}(t) - r_1 |X_{rand}(t) - 2r_2 X(t)| + \alpha \oplus L \acute{e}vy(\lambda), \ q \ge 0.5 \\ X_{rabbit}(t) - X_m(t)) - r_3 (LB + r_4 (LB + (UB - LB)) + \alpha \oplus L \acute{e}vy(\lambda), \\ q < 0.5, |E| \ge 1 \end{aligned}$$

$$(16)$$

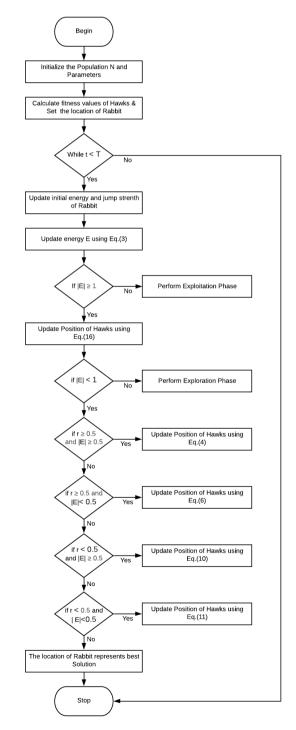


Figure 2. Flow diagram of HHO-CS

The flow diagram of HHO-CS method is displayed in Figure 2.

Table 1. Parameter settings

Algorithm	Parameter	Value
	Ν	30
HHO-CS	$p_a$	0.25
	β	1.5
HHO	N	30

<b>Table 2.</b> Results of benchmark functions $(f_1 - f_{13})$ , with 30
dimensions

f1         Avg         8.8674E-95         1.6694E-94           Std         4.8557E-94         6.9584E-94           Min         4.5074E-115         1.9980E-121           Max         2.6596E-93         3.6163E-93           f2         Avg         5.9147E-49         1.3618E-49           Min         3.3248E-59         3.4078E-59           Max         1.2151E-47         3.9850E-48           f3         Avg         2.6211E-72         8.4362E-76           Std         1.4357E-71         3.003E-75           Min         1.2370E-98         4.5853E-99           Max         7.8634E-71         1.5885E-74           f4         Avg         2.5076E-49         8.8527E-49           Std         9.4690E-49         3.6383E-48         Min           Min         6.2383E-58         4.5837E-58         Max           Max         5.0141E-48         1.9624E-47           f5         Avg         0.0290         0.0172           Std         0.0524         0.0339           Min         3.9738E-5         1.7375E-5           Max         0.2504         0.1741           f6         Avg         1.0566E-04         1.2869E-04 <th>Function</th> <th></th> <th>HHO-CS</th> <th>ННО</th>	Function		HHO-CS	ННО
Std         4.8557E-94         6.9584E-94           Min         4.5074E-115         1.9980E-121           Max         2.6596E-93         3.6163E-93           f2         Avg         5.9147E-49         1.3618E-49           Min         3.3248E-59         3.4078E-59           Max         1.2151E-47         3.9850E-48           f3         Avg         2.6211E-72         8.4362E-76           Std         1.4357E-71         3.3003E-75           Min         1.2370E-98         4.5853E-99           Max         7.8634E-71         1.5885E-74           f4         Avg         2.5076E-49         8.8527E-49           Std         9.4690E-49         3.6383E-48           Min         6.2383E-58         4.5837E-58           Max         5.0141E-48         1.9624E-47           f5         Avg         0.0290         0.0172           Std         0.0524         0.0339         Min           Min         3.9738E-5         1.7375E-5           Max         0.2504         0.1741           f6         Avg         1.0566E-04         1.2869E-04           f7         Avg         1.4913E-04         1.6149E-07 <tr< th=""><th><math>f_1</math></th><th>Avg</th><th>8.8674E-95</th><th>1.6694E-94</th></tr<>	$f_1$	Avg	8.8674E-95	1.6694E-94
Min         4.5074E-115         1.9980E-121           Max         2.6596E-93         3.6163E-93           f2         Avg         5.9147E-49         1.3618E-49           Std         2.3401E-48         7.2705E-49           Min         3.3248E-59         3.4078E-59           Max         1.2151E-47         3.9850E-48           f3         Avg         2.6211E-72         8.4362E-76           Std         1.4357E-71         3.003E-75           Min         1.2370E-98         4.5853E-99           Max         7.8634E-71         1.5885E-74           f4         Avg         2.5076E-49         8.8527E-49           Std         9.4690E-49         3.6333E-48           Min         6.2383E-58         4.5837E-58           Max         5.0141E-48         1.9624E-47           f5         Avg         0.0290         0.0172           Std         0.0524         0.0339         Min           min         3.9738E-5         1.7375E-5           Max         0.2504         0.1741           f6         Avg         1.0566E-04         1.2869E-04           f1         9.8245E-08         4.6149E-07         Max	,1		4.8557E-94	6.9584E-94
f2         Avg         5.9147E-49         1.3618E-49           Std         2.3401E-48         7.2705E-49           Min         3.3248E-59         3.4078E-59           Max         1.2151E-47         3.9850E-48           f3         Avg         2.6211E-72         8.4362E-76           Std         1.4357E-71         3.3003E-75           Min         1.2370E-98         4.5853E-99           Max         7.8634E-71         1.5885E-74           f4         Avg         2.5076E-49         8.8527E-49           Std         9.4690E-49         3.6383E-48           Min         6.2383E-58         4.5837E-58           Max         5.0141E-48         1.9624E-47           f5         Avg         0.0290         0.0172           Std         0.0290         0.0172         Std         0.0254         0.0339           Min         3.9738E-5         1.7375E-5         Max         0.2504         0.1741           f6         Avg         1.0566E-04         1.2869E-04         1.5884E-04           Min         9.8245E-08         4.6149E-07         Max         4.9675E-04         6.6066E-04           f7         Avg         1.4913E-04         <		Min		1.9980E-121
Std         2.3401E-48         7.2705E-49           Min         3.3248E-59         3.4078E-59           Max         1.2151E-47         3.9850E-48           f <sub>3</sub> Avg         2.6211E-72         8.4362E-76           Std         1.4357E-71         3.3003E-75           Min         1.2370E-98         4.5853E-99           Max         7.8634E-71         1.5885E-74           f <sub>4</sub> Avg         2.5076E-49         8.8527E-49           Std         9.4690E-49         3.6383E-48           Min         6.2383E-58         4.5837E-58           Max         5.0141E-48         1.9624E-47           f <sub>5</sub> Avg         0.0290         0.0172           Std         0.0290         0.0172         Std           Max         5.0141E-48         1.9624E-47           f <sub>5</sub> Avg         0.0290         0.0172           Std         0.0524         0.0339           Min         3.9738E-5         1.7375E-5           Max         0.2504         0.1741           f <sub>6</sub> Avg         1.2169E-04         1.5884E-04           Min         1.0482E-05         3.0423E-06           Max		Max	2.6596E-93	3.6163E-93
Std         2.3401E-48         7.2705E-49           Min         3.3248E-59         3.4078E-59           Max         1.2151E-47         3.9850E-48           f <sub>3</sub> Avg         2.6211E-72         8.4362E-76           Std         1.4357E-71         3.3003E-75           Min         1.2370E-98         4.5853E-99           Max         7.8634E-71         1.5885E-74           f <sub>4</sub> Avg         2.5076E-49         8.8527E-49           Std         9.4690E-49         3.6383E-48           Min         6.2383E-58         4.5837E-58           Max         5.0141E-48         1.9624E-47           f <sub>5</sub> Avg         0.0290         0.0172           Std         0.0290         0.0172         Std           Max         5.0141E-48         1.9624E-47           f <sub>5</sub> Avg         0.0290         0.0172           Std         0.0524         0.0339           Min         3.9738E-5         1.7375E-5           Max         0.2504         0.1741           f <sub>6</sub> Avg         1.2169E-04         1.5884E-04           Min         1.0482E-05         3.0423E-06           Max	f <sub>2</sub>	Avg	5.9147E-49	1.3618E-49
Min         3.3248E-59         3.4078E-59           Max         1.2151E-47         3.9850E-48           f <sub>3</sub> Avg         2.6211E-72         8.4362E-76           Std         1.4357E-71         3.3003E-75           Min         1.2370E-98         4.5853E-99           Max         7.8634E-71         1.5885E-74           f <sub>4</sub> Avg         2.5076E-49         8.8527E-49           Std         9.4690E-49         3.6383E-48           Min         6.2383E-58         4.5837E-58           Max         5.0141E-48         1.9624E-47           f <sub>5</sub> Avg         0.0290         0.0172           Std         0.0524         0.0339           Min         3.9738E-5         1.7375E-5           Max         0.2504         0.1741           f <sub>6</sub> Avg         1.0566E-04         1.2869E-04           Std         1.2169E-04         1.5884E-04           Min         9.8245E-08         4.6149E-07           Max         4.9675E-04         6.6066E-04           f <sub>7</sub> Avg         1.4913E-04         1.7717E-04           f <sub>8</sub> Avg         -1.2486E+04         -1.2562E+04	, 2			
Max         1.2151E-47         3.9850E-48           f <sub>3</sub> Avg         2.6211E-72         8.4362E-76           Std         1.4357E-71         3.3003E-75           Min         1.2370E-98         4.5853E-99           Max         7.8634E-71         1.5885E-74           f <sub>4</sub> Avg         2.5076E-49         8.8527E-49           Std         9.4690E-49         3.6383E-48           Min         6.2383E-58         4.5837E-58           Max         5.0141E-48         1.9624E-47           f <sub>5</sub> Avg         0.0290         0.0172           Std         0.0524         0.0339           Min         3.9738E-5         1.7375E-5           Max         0.2504         0.1741           f <sub>6</sub> Avg         1.0566E-04         1.2869E-04           Min         9.8245E-08         4.6149E-07           Max         4.9675E-04         6.6066E-04           f <sub>7</sub> Avg         1.4913E-04         1.717E-04           Std         2.0653E-04         1.4357E-04           Min         1.0482E-05         3.0423E-06           Max         8.6431E-04         6.6621E-04           f <sub>8</sub> <t< th=""><th></th><th></th><th></th><th></th></t<>				
f <sub>3</sub> Avg         2.6211E-72         8.4362E-76           Std         1.4357E-71         3.3003E-75           Min         1.2370E-98         4.5853E-99           Max         7.8634E-71         1.5885E-74           f <sub>4</sub> Avg         2.5076E-49         8.8527E-49           Std         9.4690E-49         3.6383E-48           Min         6.2383E-58         4.5837E-58           Max         5.0141E-48         1.9624E-47           f <sub>5</sub> Avg         0.0290         0.0172           Std         0.0524         0.0339           Min         3.9738E-5         1.7375E-5           Max         0.2504         0.1741           f <sub>6</sub> Avg         1.0566E-04         1.2869E-04           Std         1.2169E-04         1.5884E-04           Min         9.8245E-08         4.6149E-07           Max         4.9675E-04         6.6066E-04           f <sub>7</sub> Avg         1.4913E-04         1.7717E-04           Std         2.0653E-04         1.4357E-04           Min         1.0482E-05         3.0423E-06           Max         8.6431E-04         6.6621E-04           f <sub>8</sub>		Max	1.2151E-47	3.9850E-48
Std         1.4357E-71         3.3003E-75           Min         1.2370E-98         4.5853E-99           Max         7.8634E-71         1.5885E-74           f4         Avg         2.5076E-49         8.8527E-49           Std         9.4690E-49         3.6383E-48         Min           Min         6.2383E-58         4.5837E-58           Max         5.0141E-48         1.9624E-47           f5         Avg         0.0290         0.0172           Std         0.0524         0.0339           Min         3.9738E-5         1.7375E-5           Max         0.2504         0.1741           f6         Avg         1.0566E-04         1.2869E-04           Std         1.2169E-04         1.5884E-04           Min         9.8245E-08         4.6149E-07           Max         4.9675E-04         6.6066E-04           f7         Avg         1.4913E-04         1.7717E-04           Std         2.0653E-04         1.4357E-04         Min           Min         1.0482E-05         3.0423E-06           Max         8.6431E-04         -1.2562E+04           Max         0         0           Max         0 </th <th>f2</th> <th></th> <th></th> <th></th>	f2			
Min         1.2370E-98         4.5853E-99           Max         7.8634E-71         1.5885E-74           f4         Avg         2.5076E-49         8.8527E-49           Std         9.4690E-49         3.6383E-48           Min         6.2383E-58         4.5837E-58           Max         5.0141E-48         1.9624E-47           f5         Avg         0.0290         0.0172           Std         0.0524         0.0339           Min         3.9738E-5         1.7375E-5           Max         0.2504         0.1741           f6         Avg         1.0566E-04         1.2869E-04           Min         9.8245E-08         4.6149E-07           Max         4.9675E-04         6.6066E-04           f7         Avg         1.4913E-04         1.7717E-04           Std         2.0653E-04         1.4357E-04         Min           Min         1.0482E-05         3.0423E-06         Max           Max         71.2486E+04         -1.2562E+04         Mix           f8         Avg         -1.2486E+04         -1.2569E+04           Max         -1.2350E+04         1.2569E+04         Mix           Max         0	13			
Max         7.8634E-71         1.5885E-74           f4         Avg         2.5076E-49         8.8527E-49           Std         9.4690E-49         3.6383E-48           Min         6.2383E-58         4.5837E-58           Max         5.0141E-48         1.9624E-47           f5         Avg         0.0290         0.0172           std         0.0524         0.0339           Min         3.9738E-5         1.7375E-5           Max         0.2504         0.1741           f6         Avg         1.0566E-04         1.2869E-04           Min         9.8245E-08         4.6149E-07           Max         4.9675E-04         6.6066E-04           f7         Avg         1.4913E-04         1.7717E-04           f8         Avg         -1.2486E+04         -1.2562E+04           Min         1.0482E-05         3.0423E-06           Max         -1.2569E+04         1.2569E+04           f9         Avg         0         0           Min         0         0         0           Min         0         0         0           Max         3.8818E-16         8.8818E-16           Max         0				
f4         Avg         2.5076E-49         8.8527E-49           Std         9.4690E-49         3.6383E-48           Min         6.2383E-58         4.5837E-58           Max         5.0141E-48         1.9624E-47           f5         Avg         0.0290         0.0172           Std         0.0524         0.0339         Min           Min         3.9738E-5         1.7375E-5           Max         0.2504         0.1741           f6         Avg         1.0566E-04         1.2869E-04           Min         9.8245E-08         4.6149E-07           Max         4.9675E-04         6.6066E-04           f7         Avg         1.4913E-04         1.7717E-04           Std         2.0653E-04         1.4357E-04           Min         1.0482E-05         3.0423E-06           Max         8.6431E-04         6.6621E-04           f8         Avg         -1.2486E+04         -1.2569E+04           f9         Avg         0         0           Min         -1.2569E+04         1.2350E+04           Max         -1.2350E+04         1.2350E+04           f9         Avg         0         0				
Std         9.4690E-49         3.6383E-48           Min         6.2383E-58         4.5837E-58           Max         5.0141E-48         1.9624E-47           f5         Avg         0.0290         0.0172           Std         0.0524         0.0339           Min         3.9738E-5         1.7375E-5           Max         0.2504         0.1741           f6         Avg         1.0566E-04         1.2869E-04           Min         9.8245E-08         4.6149E-07           Max         4.9675E-04         6.6066E-04           f7         Avg         1.4913E-04         1.7717E-04           Std         2.0653E-04         1.4357E-04           Min         1.0482E-05         3.0423E-06           Max         8.6431E-04         6.6621E-04           f8         Avg         -1.2486E+04         -1.2569E+04           Max         -1.2350E+04         1.2350E+04         1.2350E+04           Max         -1.2350E+04         1.2350E+04         1.2350E+04           f9         Avg         0         0         0           Min         0         0         0         0           Max         0         0 <th>f,</th> <th></th> <th></th> <th></th>	f,			
Min         6.2383E-58         4.5837E-58           Max         5.0141E-48         1.9624E-47           f5         Avg         0.0290         0.0172           Std         0.0524         0.0339           Min         3.9738E-5         1.7375E-5           Max         0.2504         0.1741           f6         Avg         1.0566E-04         1.2869E-04           Min         9.8245E-08         4.6149E-07           Max         4.9675E-04         6.6066E-04           f7         Avg         1.4913E-04         1.7717E-04           Std         2.0653E-04         1.4357E-04           Min         1.0482E-05         3.0423E-06           Max         8.6431E-04         6.6621E-04           f8         Avg         -1.2486E+04         -1.2569E+04           Max         8.6431E-04         6.6621E-04           f9         Avg         0         0           Max         -1.2350E+04         1.2350E+04           Max         -1.2569E+04         1.2569E+04           f9         Avg         0         0           Min         0         0         0           Max         0	<b>J</b> 4			
Max         5.0141E-48         1.9624E-47           f5         Avg         0.0290         0.0172           Std         0.0524         0.0339           Min         3.9738E-5         1.7375E-5           Max         0.2504         0.1741           f6         Avg         1.0566E-04         1.2869E-04           Min         9.8245E-08         4.6149E-07           Max         4.9675E-04         6.6066E-04           f7         Avg         1.4913E-04         1.7717E-04           Std         2.0653E-04         1.4357E-04           Min         1.0482E-05         3.0423E-06           Max         8.6431E-04         6.6621E-04           f8         Avg         -1.2486E+04         -1.2562E+04           Max         45.2858         40.0058           Min         -1.2569E+04         1.2350E+04           f9         Avg         0         0           Max         0         0         0           Min         0         0         0           Max         0         0         0           Max         0         0         0           Max         0         0				
f5         Avg         0.0290         0.0172           Std         0.0524         0.0339           Min         3.9738E-5         1.7375E-5           Max         0.2504         0.1741           f6         Avg         1.0566E-04         1.2869E-04           Std         1.2169E-04         1.5884E-04           Min         9.8245E-08         4.6149E-07           Max         4.9675E-04         6.6066E-04           f7         Avg         1.4913E-04         1.7717E-04           Std         2.0653E-04         1.4357E-04         Min           Min         1.0482E-05         3.0423E-06         Max           Max         8.6431E-04         6.6621E-04         f8           Max         -1.2569E+04         -1.2569E+04         1.2350E+04           Max         -1.2350E+04         1.2350E+04         1.2350E+04           f9         Avg         0         0         0           Min         0         0         0         0           Min         0         0         0         0           Max         0         0         0         0           Max         0         0				
Std         0.0524         0.0339           Min         3.9738E-5         1.7375E-5           Max         0.2504         0.1741           f6         Avg         1.0566E-04         1.2869E-04           Std         1.2169E-04         1.5884E-04           Min         9.8245E-08         4.6149E-07           Max         4.9675E-04         6.6066E-04           f7         Avg         1.4913E-04         1.7717E-04           Std         2.0653E-04         1.4357E-04           Min         1.0482E-05         3.0423E-06           Max         8.6431E-04         6.6621E-04           f8         Avg         -1.2486E+04         -1.2562E+04           Max         -1.2350E+04         1.2350E+04         1.2350E+04           f9         Avg         0         0           Min         0         0         0           Min         0         0         0           f10         Avg         8.8818E-16         8.8818E-16           f11         Avg         0         0           Min         8.8818E-16         8.8818E-16           f11         Avg         0         0 <td< th=""><th>f_</th><th></th><th></th><th></th></td<>	f_			
Min         3.9738E-5         1.7375E-5           Max         0.2504         0.1741           f <sub>6</sub> Avg         1.0566E-04         1.2869E-04           Std         1.2169E-04         1.5884E-04           Min         9.8245E-08         4.6149E-07           Max         4.9675E-04         6.6066E-04           f <sub>7</sub> Avg         1.4913E-04         1.7717E-04           Std         2.0653E-04         1.4357E-04           Min         1.0482E-05         3.0423E-06           Max         8.6431E-04         6.6621E-04           f <sub>8</sub> Avg         -1.2486E+04         -1.2562E+04           Max         45.2858         40.0058           Min         -1.2569E+04         1.2350E+04           f <sub>9</sub> Avg         0         0           Max         0         0         0           Min         0         0         0           Min         0         0         0           Max         0         0         0           f         Avg         0         0           Min         8.8818E-16         8.8818E-16           f         Max         8	<b>J</b> 5			
Max         0.2504         0.1741           f_6         Avg         1.0566E-04         1.2869E-04           Std         1.2169E-04         1.5884E-04           Min         9.8245E-08         4.6149E-07           Max         4.9675E-04         6.6066E-04           f7         Avg         1.4913E-04         1.717E-04           Std         2.0653E-04         1.4357E-04         Min           Min         1.0482E-05         3.0423E-06         Max           Max         8.6431E-04         6.6621E-04         fs           Max         -1.2569E+04         -1.2562E+04         Moto58           Min         -1.2569E+04         1.2350E+04         1.2350E+04           fg         Avg         0         0         0           Max         0         0         0         0           Min         0         0         0         0           Max         0         0         0         0           Min </td <td></td> <td></td> <td></td> <td></td>				
f <sub>6</sub> Avg         1.0566E-04         1.2869E-04           Std         1.2169E-04         1.5884E-04           Min         9.8245E-08         4.6149E-07           Max         4.9675E-04         6.6066E-04           f <sub>7</sub> Avg         1.4913E-04         1.7717E-04           Std         2.0653E-04         1.4357E-04         Min           Min         1.0482E-05         3.0423E-06         Max           Max         8.6431E-04         6.6621E-04         fs           Max         -1.2486E+04         -1.2562E+04         Moto58           Min         -1.2569E+04         1.2350E+04         1.2350E+04           Max         -1.2350E+04         1.2350E+04         1.2350E+04           f <sub>9</sub> Avg         0         0         0           Min         0         0         0         0           Max         0         0         0         0           Min         8.8818E-16         8.8818E-16         8				
Std         1.2169E-04         1.5884E-04           Min         9.8245E-08         4.6149E-07           Max         4.9675E-04         6.6066E-04           f7         Avg         1.4913E-04         1.7717E-04           Std         2.0653E-04         1.4357E-04           Min         1.0482E-05         3.0423E-06           Max         8.6431E-04         6.6621E-04           f8         Avg         -1.2486E+04         -1.2562E+04           Min         -1.2350E+04         1.2569E+04           Max         -1.2350E+04         1.2350E+04           f9         Avg         0         0           Min         0         0         0           Max         0         0         0           Min         8.8818E-16         8.8818E-16         1.47E+02           Min         8.8818E-16         8.8818E-16         1.300E-05           Min         0         0         0           <	f			
Min         9.8245E-08         4.6149E-07           Max         4.9675E-04         6.6066E-04           f7         Avg         1.4913E-04         1.7717E-04           Std         2.0653E-04         1.4357E-04         Min           Min         1.0482E-05         3.0423E-06         Max           Max         8.6431E-04         6.6621E-04         fs           Min         -1.2486E+04         -1.2562E+04         Std           Min         -1.2569E+04         1.2569E+04         1.2350E+04           Max         -1.2350E+04         1.2350E+04         1.2350E+04           fg         Avg         0         0         0           Min         0         0         0         0           Min         0         0         0         0           Min         0         0         0         0           Max         0         0         0         0           Max         0         0         0         0           Max         0         0         0         0           Min         8.8818E-16         8.8818E-16         1.47E+02           Min         8.8818E-16         8.8818E-16 </th <th><b>J</b> 6</th> <th></th> <th></th> <th></th>	<b>J</b> 6			
Max         4.9675E-04         6.6066E-04           f7         Avg         1.4913E-04         1.7717E-04           Std         2.0653E-04         1.4357E-04           Min         1.0482E-05         3.0423E-06           Max         8.6431E-04         6.6621E-04           f8         Avg         -1.2486E+04         -1.2562E+04           Std         45.2858         40.0058           Min         -1.2569E+04         1.2350E+04           f9         Avg         0         0           Max         -1.2350E+04         1.2350E+04         1.2350E+04           f9         Avg         0         0         0           Min         0         0         0         0           Min         0         0         0         0           Max         0         0         0         0           Max         0         0         0         0           Max         0         0         0         0           Min         8.8818E-16         8.8818E-16         5.8818E-16           Min         8.8818E-16         8.8818E-16         5.8818E-16           Max         8.8818E-16         8				
f7         Avg         1.4913E-04         1.7717E-04           Std         2.0653E-04         1.4357E-04           Min         1.0482E-05         3.0423E-06           Max         8.6431E-04         6.6621E-04           f8         Avg         -1.2486E+04         -1.2562E+04           Std         45.2858         40.0058           Min         -1.2569E+04         1.2569E+04           Max         -1.2350E+04         1.2350E+04           f9         Avg         0         0           Min         0         0         0           Max         0         0         0           f10         Avg         8.8818E-16         8.8818E-16           Min         8.8818E-16         8.8818E-16         f.1300E-05           Std         0         0         0           Min         0         0         0           Max </th <th></th> <th></th> <th></th> <th></th>				
Std         2.0653E-04         1.4357E-04           Min         1.0482E-05         3.0423E-06           Max         8.6431E-04         6.6621E-04           f <sub>8</sub> Avg         -1.2486E+04         -1.2562E+04           Std         45.2858         40.0058           Min         -1.2569E+04         1.2569E+04           Max         -1.2350E+04         1.2350E+04           f <sub>9</sub> Avg         0         0           Min         0         0         0           Max         0         0         0           Min         8.8818E-16         8.8818E-16         8.8818E-16           Max         8.8818E-16         8.8818E-16         5.8818E-16           Min         8.8818E-16         8.8818E-16         5.8818E-16           Min         0         0         0         0           Min         0         0         0         0           Max         8.8818E-16	f			
Min         1.0482E-05         3.0423E-06           Max         8.6431E-04         6.6621E-04           f <sub>8</sub> Avg         -1.2486E+04         -1.2562E+04           Std         45.2858         40.0058           Min         -1.2569E+04         1.2569E+04           Max         -1.2350E+04         1.2350E+04           f <sub>9</sub> Avg         0         0           Min         0         0         0           Min         0         0         0           Min         0         0         0           Min         0         0         0           Max         0         0         0           Min         8.8818E-16         8.8818E-16         8.8818E-16           Std         1.47E+02         1.47E+02         1.47E+02           Min         8.8818E-16         8.8818E-16         5.8818E-16           Max         8.8818E-16         8.8818E-16         5.8818E-16           Max         8.8818E-16         8.8818E-16         5.818           f11         Avg         0         0         0           Min         0         0         0         0 <td< th=""><th><b>J</b>7</th><th></th><th></th><th></th></td<>	<b>J</b> 7			
Max         8.6431E-04         6.6621E-04           f <sub>8</sub> Avg         -1.2486E+04         -1.2562E+04           Std         45.2858         40.0058           Min         -1.2569E+04         1.2569E+04           Max         -1.2350E+04         1.2569E+04           f <sub>9</sub> Avg         0         0           f <sub>10</sub> Avg         0         0           Min         0         0         0           f <sub>10</sub> Avg         8.8818E-16         8.8818E-16           Std         1.47E+02         1.47E+02           Min         8.8818E-16         8.8818E-16           Max         0         0           Min         8.8818E-16         8.8818E-16           Max         8.8818E-16         8.8818E-16           Max         0         0           Min         8.8818E-16         8.8818E-16           f <sub>11</sub> Avg         0         0           Min         0         0         0           Min         0         0         0           Max         0         0         0           Min         0         0         0 <t< th=""><th></th><th></th><th></th><th></th></t<>				
f <sub>8</sub> Avg         -1.2486E+04         -1.2562E+04           Std         45.2858         40.0058           Min         -1.2569E+04         1.2569E+04           Max         -1.2350E+04         1.2350E+04           f <sub>9</sub> Avg         0         0           Min         0         0         0           Min         0         0         0           Max         0         0         0           Min         0         0         0           Max         0         0         0           Max         0         0         0           Max         0         0         0           f10         Avg         8.8818E-16         8.8818E-16           Max         8.8818E-16         8.8818E-16         1.47E+02           Min         8.8818E-16         8.8818E-16         1.47E+02           Min         8.8818E-16         8.8818E-16         1.47E+02           Min         0         0         0           Max         0.88918E-16         1.1300E-05         Std           Min         0         0         0           Max         0         0 <th></th> <th></th> <th></th> <th></th>				
Std         45.2858         40.0058           Min         -1.2569E+04         1.2569E+04           Max         -1.2350E+04         1.2350E+04           fg         Avg         0         0           Min         0         0         0           Min         0         0         0           Max         0         0         0           Min         0         0         0           Max         0         0         0           f10         Avg         8.8818E-16         8.8818E-16           Std         1.47E+02         1.47E+02           Min         8.8818E-16         8.8818E-16           Max         0         0           Max         8.8818E-16         8.8818E-16           f11         Avg         0         0           Min         0         0         0           Min         0         0         0           Min         0         0         0           Max         0         0         0           Min         0         0         0           f12         Avg         5.9841E-06         1.1300E-05 <th>£</th> <th></th> <th></th> <th></th>	£			
Min         -1.2569E+04         1.2569E+04           Max         -1.2350E+04         1.2350E+04           f <sub>9</sub> Avg         0         0           Min         0         0         0           Min         0         0         0           Max         0         0         0           Min         0         0         0           f10         Avg         8.8818E-16         8.8818E-16           Std         1.47E+02         1.47E+02           Min         8.8818E-16         8.8818E-16           Max         0         0           Min         8.8818E-16         8.8818E-16           Max         0.0         0           Std         0         0           Min         0         0           Min         0         0           Min         0         0           Min         0         0           Max         3.4656E-05         1.1300E-05      <	<b>J</b> 8			
Max         -1.2350E+04         1.2350E+04           f <sub>9</sub> Avg         0         0           Std         0         0           Min         0         0           Max         0         0           f <sub>10</sub> Avg         8.8818E-16         8.8818E-16           Std         1.47E+02         1.47E+02           Min         8.8818E-16         8.8818E-16           Max         0         0           Min         8.8818E-16         8.8818E-16           Max         0.0         0           Max         0.0         0           Max         0.0         0           Std         0         0           Min         0         0           Min         0         0           Max         0         0           Max         0         0           Max         0         0           f12         Avg         5.9841E-06         1.1300E-05           Std         9.2809E-06         2.2354E-05           Min         1.4347E-08         7.8338E-09           Max         3.4656E-05         1.1656E-04 <t< th=""><th></th><th></th><th></th><th></th></t<>				
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Std         0         0           Min         0         0           Max         0         0           f10         Avg         8.8818E-16         8.8818E-16           Std         1.47E+02         1.47E+02           Min         8.8818E-16         8.8818E-16           Max         8.8818E-16         8.8818E-16           Max         8.8818E-16         8.8818E-16           f11         Avg         0         0           Min         0         0         0           Max         0         0         0           f12         Avg         5.9841E-06         1.1300E-05           Std         9.2809E-06         2.2354E-05           Min         1.4347E-08         7.8338E-09           Max         3.4656E-05         1.1656E-04           f13         Avg         7.0957E-05         8.1648E-05           Std         1.2754E-04         9.4889E-05	f			
Min         0         0           Max         0         0           f10         Avg         8.8818E-16         8.8818E-16           Std         1.47E+02         1.47E+02           Min         8.8818E-16         8.8818E-16           Max         8.8818E-16         8.8818E-16           f11         Avg         0         0           Std         0         0         0           Min         1.4347E-06         1.1300E-05         Std           Std         9.2809E-06         2.2354E-05         Min           Min         1.4347E-08         7.8338E-09         Max           Max         3.4656E-05         1.1656E-04         4           f13         Avg         7.0957E-05         8.1648E-05           Std         1.2754E-04         9.4889E-05         Min           Min         2.4497E-08         5.8620E-09         1.497540-04	<b>J</b> 9			
Max         0         0           f10         Avg         8.8818E-16         8.8818E-16           Std         1.47E+02         1.47E+02           Min         8.8818E-16         8.8818E-16           Max         8.8818E-16         8.8818E-16           f11         Avg         0         0           Std         0         0         0           Min         0         0         0           Min         0         0         0           Max         0         0         0           f12         Avg         5.9841E-06         1.1300E-05           Std         9.2809E-06         2.2354E-05           Min         1.4347E-08         7.8338E-09           Max         3.4656E-05         1.1656E-04           f13         Avg         7.0957E-05         8.1648E-05           Std         1.2754E-04         9.4889E-05           Min         2.4497E-08         5.				
f10         Avg         8.8818E-16         8.8818E-16           Std         1.47E+02         1.47E+02           Min         8.8818E-16         8.8818E-16           Max         8.8818E-16         8.8818E-16           f11         Avg         0         0           Min         0         0         0           Max         0         0         0           Max         0         0         0           Max         0         0         0           Max         0         0         0           f12         Avg         5.9841E-06         1.1300E-05           Std         9.2809E-06         2.2354E-05           Min         1.4347E-08         7.8338E-09           Max         3.4656E-05         1.1656E-04           f13         Avg         7.0957E-05         8.1648E-05           Std         1.2754E-04         9.4889E-05           Min         2.4497E-08<				
Std         1.47E+02         1.47E+02           Min         8.8818E-16         8.8818E-16           Max         8.8818E-16         8.8818E-16           f11         Avg         0         0           Std         0         0         0           Min         0         0         0           Min         0         0         0           Max         0         0         0           Max         0         0         0           f12         Avg         5.9841E-06         1.1300E-05           Std         9.2809E-06         2.2354E-05           Min         1.4347E-08         7.8338E-09           Max         3.4656E-05         1.1656E-04           f13         Avg         7.0957E-05         8.1648E-05           Std         1.2754E-04         9.4889E-05           Min         2.4497E-08         5.8620E-09	f			
Min         8.8818E-16 8.8818E-16         8.8818E-16 8.8818E-16           f <sub>11</sub> Avg         0         0           Std         0         0         0           Min         0         0         0           Max         5.9841E-06         1.1300E-05         5.8138E-09           f12         Avg         5.9841E-06         1.1300E-05           Min         1.4347E-08         7.8338E-09           Max         3.4656E-05         1.1656E-04           f13         Avg         7.0957E-05         8.1648E-05           Std         1.2754E-04         9.4889E-05           Min         2.4497E-08         5.8620E-09	<b>J</b> 10			
Max         8.8818E-16         8.8818E-16           f <sub>11</sub> Avg         0         0           Std         0         0         0           Min         0         0         0           Max         0.8818E-16         1.1300E-05         0           f12         Avg         5.9841E-06         1.1300E-05           Std         9.2809E-06         2.2354E-05         Min           Max         3.4656E-05         1.1656E-04           f13         Avg         7.0957E-05         8.1648E-05           Std         1.2754E-04         9.4889E-05           Min         2.4497E-08         5.8620E-09				
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Std         0         0           Min         0         0           Max         0         0           f12         Avg <b>5.9841E-06</b> 1.1300E-05           Std         9.2809E-06         2.2354E-05           Min         1.4347E-08         7.8338E-09           Max         3.4656E-05         1.1656E-04           f13         Avg <b>7.0957E-05</b> 8.1648E-05           Std         1.2754E-04         9.4889E-05           Min         2.4497E-08         5.8620E-09	£			
Min         0         0           Max         0         0           f12         Avg         5.9841E-06         1.1300E-05           Std         9.2809E-06         2.2354E-05           Min         1.4347E-08         7.8338E-09           Max         3.4656E-05         1.1656E-04           f13         Avg         7.0957E-05         8.1648E-05           Std         1.2754E-04         9.4889E-05           Min         2.4497E-08         5.8620E-09	<b>J</b> 11			
Max         0         0           f12         Avg <b>5.9841E-06</b> 1.1300E-05           Std         9.2809E-06         2.2354E-05           Min         1.4347E-08         7.8338E-09           Max         3.4656E-05         1.1656E-04           f13         Avg <b>7.0957E-05</b> 8.1648E-05           Std         1.2754E-04         9.4889E-05           Min         2.4497E-08         5.8620E-09				
f <sub>12</sub> Avg <b>5.9841E-06</b> 1.1300E-05           Std         9.2809E-06         2.2354E-05           Min         1.4347E-08         7.8338E-09           Max         3.4656E-05         1.1656E-04 <b>f</b> <sub>13</sub> Avg <b>7.0957E-05</b> 8.1648E-05           Std         1.2754E-04         9.4889E-05           Min         2.4497E-08         5.8620E-09				
Std         9.2809E-06         2.2354E-05           Min         1.4347E-08         7.8338E-09           Max         3.4656E-05         1.1656E-04           f <sub>13</sub> Avg         7.0957E-05         8.1648E-05           Std         1.2754E-04         9.4889E-05           Min         2.4497E-08         5.8620E-09	£			
Min         1.4347E-08         7.8338E-09           Max         3.4656E-05         1.1656E-04           f13         Avg         7.0957E-05         8.1648E-05           Std         1.2754E-04         9.4889E-05           Min         2.4497E-08         5.8620E-09	J 12			
Max         3.4656E-05         1.1656E-04           f <sub>13</sub> Avg         7.0957E-05         8.1648E-05           Std         1.2754E-04         9.4889E-05           Min         2.4497E-08         5.8620E-09				
f <sub>13</sub> Avg         7.0957E-05         8.1648E-05           Std         1.2754E-04         9.4889E-05           Min         2.4497E-08         5.8620E-09				
Std         1.2754E-04         9.4889E-05           Min         2.4497E-08         5.8620E-09				
Min 2.4497E-08 5.8620E-09	$f_{13}$			
Max 6.3517E-04 3.5137E-04		Min		
		Max	6.3517E-04	3.5137E-04

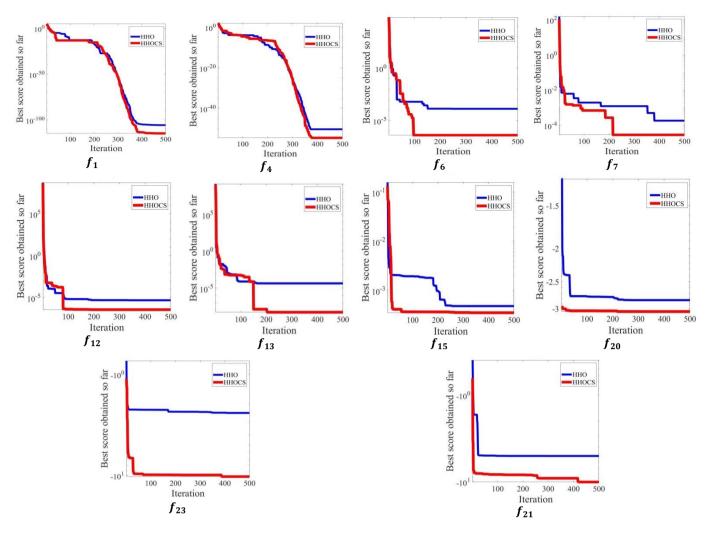


Figure 3. Convergence curves of HHO-CS and HH

**Table 3.** Results of benchmark functions  $(f_{14}-f_{23})$ 

Function		HHO-CS	HHO
$f_{14}$	Avg	1.5585	1.3280
	Std	1.2876	0.9466
	Min	0.9980	0.9980
	Max	5.9288	5.9288
$f_{15}$	Avg	3.4236E-04	3.8963E-04
	Std	2.9925E-05	2.6287E-04
	Min	3.0756E-04	3.0771E-04
	Max	4.4702E-04	1.8000E-03
$f_{16}$	Avg	-1.0316	-1.0316
	Std	6.78E-16	6.78E-16
	Min	-1.0316	-1.0316
	Max	-1.0316	-1.0316
$f_{17}$	Avg	0.3979	0.3979
	Std	2.54E-06	2.54E-06
	Min	0.3979	0.3979
	Max	0.3979	0.3979
$f_{18}$	Avg	3	3
	Std	0	0
	Min	3	3
	Max	3	3
$f_{19}$	Avg	-3.6028	-3.8590
	Std	1.4095	0.0061
	Min	-3.8628	-3.8628
	Max	-3.8599	-3.8333
$f_{20}$	Avg	-3.1250	-3.0913
	Std	0.0726	0.0988
	Min	-3.2605	-3.2836
	Max	-2.9690	-2.8111

$f_{21}$	Avg	-5.5267	-5.1375
	Std	1.4608	1.0277
	Min	-10.0063	-10.0464
	Max	-5.0028	-2.6226
$f_{22}$	Avg	-5.2484	-5.2495
	Std	0.9042	0.9097
	Min	-10.0360	-10.0658
	Max	-5.0679	-5.0685
$f_{23}$	Avg	-5.4583	-5.3041
	Std	1.2722	0.9876
	Min	-10.4055	-10.5332
	Max	-5.1106	-5.1076

#### **Benchmark Function Optimization**

To test the effectiveness of HHO-CS, HHO, and CS algorithms, a set of 23 standard benchmark functions including unimodal, multimodal, multimodal with fixed dimension functions ( $f_1 - f_{23}$ ) are taken for a minimization problem. The unimodal functions are used to test the exploitation capability of optimizers and the multimodal functions are used to test the exploration ability. The unimodal functions also signify the ability to reach the global best while the performance of the multimodal functions size is set to 30. The population size N is 30 and the maximum iteration is 500. All the algorithms are run in MATLAB R2018 having an Intel Core i5-8265U CPU clocked at 1.60GHz with 4GB RAM, with windows 10 operating system. The parameter settings are shown in Table 1. The results of an Average (Avg), Standard deviation (Std), Minima

(Min) and Maxima (Max) of 30 runs of each benchmark functions are shown in Table 2&3. The boldface letters indicate the best results. The convergence curves are shown in Figure 3.

In summary, the proposed HHO-CS algorithm performs better than the HHO for the multimodal test functions. However, the performance of our method is similar to that of the HHO for some of the functions. Nevertheless, the suggested algorithm ensures a better convergence, because of its enhanced exploitation capability.

#### 4. METHODOLOGY

Multilevel thresholding of color thermogram images is solved using the RGB histogram as the input, considering that the color images contain more information, better visual perception of the human eye with contrary to grayscale images, where we cannot see the temperature variations. The multilevel thresholding technique is used to get better results.

#### 4.1 Otsu's between class variance

The bi-level and multilevel thresholding of images based on the between class variance was first proposed by Otsu [18]. Bi-level thresholding and multilevel thresholding separate images into classes when the maximum variance is calculated. This method considers histogram of an image as an input. The probability distribution of intensity levels of R, G, B channel is obtained. The optimal threshold values are obtained for each channel of the colour image. The mathematical representation is given below

$$\sigma^{2} = \sum_{k=1}^{m} \sigma_{k} = \sum_{k=1}^{m} \omega_{k} (\mu_{k} - \mu_{r})^{2}$$
(17)

$$\mu_{k} = \sum_{i=thk}^{th_{k+1}-1} \frac{kPE_{i}}{\omega_{i}(th_{i})}$$
(18)

where,

$$\omega_k = \sum_{i=th_k}^{th_{k+1}-1} PE_i \tag{19}$$

$$f_{otsu}(th) = \max(\sigma^2(th)), \ 0 \le th \le L - 1$$
(20)

where,  $\sigma^2$  is the variance,  $\mu$  is the mean.

#### 4.2 Kapur's entropy

Kapur's entropy method measures the entropy of different classes of an image. To segment colour images, the Kapur's entropy maximizes the entropy and obtain optimal threshold values of each R, G, B channel. The probability distribution of intensity levels of each R, G, B channel is used to measure the entropy criterion. Segmentation of Colour images performed by maximizing Kapur's entropy, which is taken as the objective function [19]. The mathematical formulations for Kapur's entropy are

$$f_{\kappa_{apur}}(th) = \max\left(\sum_{k=1}^{m} H_k\right)$$
(21)

where, entropy of each class is calculated by

$$H_{k} = \sum_{i=thk}^{thk+i-1} \frac{PE_{i}}{\omega_{k}} \ln\left(\frac{PE_{i}}{\omega_{k}}\right)$$
(22)

In summary, the proposed Harris Hawks-Cuckoo Search Optimizer (Eq. (16)) is used to optimize the fitness functions shown in Eq. (20) (Otsu's method) and Eq. (21) (Kapur's method). It is reiterated that the optimum threshold values are obtained through the maximization.

#### 5. RESULTS AND DISCUSSIONS

The multilevel colour thermogram image thresholding method is implemented using both Otsu's between-class variance and Kapur's entropy as the fitness functions. The proposed HHO-CS, CS and HHO algorithms are implemented to get optimal results. The multilevel colour thermogram image thresholding method is shown in Figure 4.

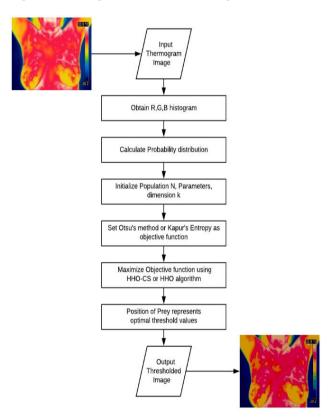


Figure 4. Multilevel thresholding of thermal images

The benchmark images are displayed in Figure 5. The experiments are based on a set of 8 different images acquired from the Database for Research Mastology with Infrared images [20]. The images are captured using a FLIR SC-620 Thermal Camera. The selected images and their respective histogram plots are described in Figure 5. For experimental purposes, images with size  $341 \times 256$  are taken.

The population size and the maximum number of iterations of each algorithm are set to 30 and 500, respectively. The Lower bound (LB) and upper bound (UB) of the algorithm is set to 0 to 255. The performance of the algorithms is evaluated, which is composed of 20 runs of the same algorithm using a specific image and calculating the average of objective function values, PSNR, SSIM and FSIM [21-24].

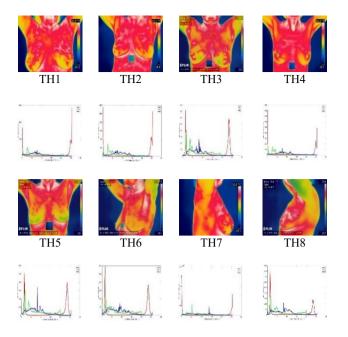


Figure 5. Benchmark images and their respective histograms

#### 5.1 Benchmark images

The Peak Signal to noise ratio (PSNR) is a widely used

performance metric for measuring the quality of the original image with the reconstructed images. Structure Similarity Index (SSIM) and Feature Similarity index (FSIM) quality metric measure the similarity between the original image and the output segmented image. SSIM specify quality degradation due to data processing. All experiments are performed on MATLAB R2018a with 4GB RAM on an Intel core i5 CPU clocked at 1.6 GHz frequency.

#### 5.2 Experiment 1: Based on Otsu's between class variance

Optimal threshold values are obtained using HHO-CS algorithm and presented in Table 4. Objective function values and PSNR values obtained from HHO-CS and HHO algorithms using Otsu's between class variance are displayed in Table 5. Remarkable differences are found. It is observed that the suggested HHO-CS method outperforms as compared to HHO. Similarly, a significant improvement over the HHO algorithm is seen with respect to the PSNR values. The reason could be the enhanced exploitation capability of HHO-CS method to get the best solutions. For instance, an improvement of 3% in PSNR value is seen in the test image sample TH1 with threshold level K=4 (see Table 5). The SSIM and FSIM values obtained from HHO-CS and HHO algorithms using Otsu's between-class variance are shown in Table 6. Interestingly, the suggested technique has shown better values (for SSIM and FSIM) than HHO.

Table 4. Threshold values obtained using HHO-CS algorithm

Image	K		HHO-CS	
		R	G	В
TH1	2	137,239	110,210	82,163
	3	141,176,230	60,153,182	62,130,149
	4	44,58,113,145	44,102,160,230	46,86,135,250
	5	145,191,196,197,254	61,87,168,173,255	83,98,152,196,236
TH2	2	138,236	82,88	81,190
	3	108,212,228	62,60,140	51,86,118
	4	101,155,176,255	93,130,167,228	46,94,185,198
	5	112,180,183,224,255	83,96,126,200,247	82,128,137,239,254
TH3	2	125,229	102,238	83,86
	3	136,147,180	81,151,215	63,110,196
	4	140,188,212,249	59,91,140,243	63,104,195,248
	5	32,153,155,190,249	83,96,97,103,231	60,76,86,164,196
TH4	2	148,203	95,174	77,90
	3	100,189,222	56,130,217	52,107,108
	4	104,164,194,250	110,148,175,251	80,114,190,215
	5	106,111,184,249,254	64,69,88,123,217	58,88,64,65,104
TH5	2	137,138	101,209	75,88
	3	113,141,201	60,134,141	47,63,126
	4	155,162,172,254	112,146,147,219	84,94,202,215
	5	130,165,192,217,253	86,166,174,187,218	76,96,176,209,220
TH6	2	128,137	47,100	85,147
	3	117,134,206	56,131,209	71,138,166
	4	130,143,170,254	118,120,126,216	60,117,202,244
	5	66,185,195,199,245	94,107,119,148,208	55,84,93,162,247
TH7	2	139,184	93,97	56,85
	3	115,124,214	63,136,158	59,61,129
	4	219,237,241,251	110,167,184,232	91,120,243,246
	5	114,118,142,250,255	78,138,186,191,240	29,68,92,133,207
TH8	2	125,139	100,126	92,130
	3	97,190,243	43,64,131	54,83,169
	4	125,156,162,253	126,134,218,233	94,95,131,213
	5	141,156,159,213,247	93,115,182,238,253	21,63,98,241,247

		OBJECTIVE	FUNCTION	PSN	IR
Images	K	HHO-CS	ННО	HHO-CS	HHO
TH1	2	1.3864 E+04	1.3829E+04	55.0114	53.4132
	3	1.4623 E+04	1.4581E+04	62.7343	62.5010
	4	1.7680 E+04	1.7483E+04	69.6979	67.6563
	5	1.9050 E+04	1.8744E+04	74.3875	73.3842
TH2	2	1.5874 E+04	1.5860E+04	55.3194	54.1919
	3	1.6509 E+04	1.6499E+04	62.4648	61.3768
	4	1.9470 E+04	1.8832E+04	66.3321	65.7321
	5	2.0844 E+04	1.9810E+04	72.0098	71.8845
TH3	2	1.2160 E+04	1.2133E+04	55.3793	53.9000
	3	1.3104 E+04	1.3012E+04	62.1599	60.9659
	4	1.8422 E+04	1.7919E+04	65.2385	64.2440
	5	2.0441 E+04	1.8662E+04	68.4839	66.8464
TH4	2	1.6818 E+04	1.6807E+04	56.1415	54.938
	3	1.7437 E+04	1.7369E+04	58.5895	55.1351
	4	2.1086 E+04	1.9552E+04	64.3450	60.9177
	5	2.2654 E+04	2.1593E+04	66.0842	64.0399
TH5	2	1.2864 E+04	1.2858E+04	56.2041	55.5316
	3	1.3962 E+04	1.3833E+04	57.7679	56.0270
	4	1.8368 E+04	1.7688E+04	59.3859	58.7054
	5	2.0739 E+04	1.9943E+04	62.8876	61.4830
TH6	2	1.4484 E+04	1.4467E+04	56.5041	55.0818
	3	1.5325 E+04	1.5185E+04	58.1370	57.5004
	4	2.0903 E+04	2.0314E+04	64.2811	63.2488
	5	2.2077 E+04	2.1627E+04	66.2539	65.4236
TH7	2	1.8836 E+04	1.8825E+04	57.6207	55.0971
	3	1.9405 E+04	1.9340E+04	63.8870	62.9271
	4	2.2614 E+04	2.1881E+04	65.7686	63.9271
	5	2.5290 E+04	2.3362E+04	66.2036	65.7404
TH8	2	1.4799 E+04	1.4757E+04	57.6318	56.5587
	3	1.5705 E+04	1.5658E+04	64.2626	64.2060
	4	2.1482 E+04	2.1221E+04	67.8773	67.5404
	5	2.2905 E+04	2.2280E+04	69.2639	68.6456

 Table 5. Comparison of objective function and PSNR values

 obtained from HHO-CS and HHO algorithms using Otsu's

 between-class variance

**Table 6.** Comparison of SSIM and FSIM values obtainedfrom HHO-CS and HHO algorithms using Otsu's betweenclass variance

		SSI	M	FSI	M
Images	K	HHO-CS	HHO	HHO-CS	HHO
TH1	2	0.7342	0.6967	0.7515	0.7486
	3	0.7829	0.7355	0.8029	0.7992
	4	0.8280	0.8181	0.8140	0.8110
	5	0.8604	0.8523	0.8396	0.8347
TH2	2	0.7114	0.6912	0.7586	0.7170
	3	0.8079	0.7904	0.7946	0.7781
	4	0.8501	0.8483	0.8267	0.8231
	5	0.9109	0.8976	0.8438	0.8362
TH3	2	0.7281	0.7060	0.7676	0.7468
	3	0.7964	0.7784	0.8025	0.7970
	4	0.8248	0.8174	0.8238	0.8258
	5	0.8787	0.8653	0.8449	0.8418
TH4	2	0.6699	0.6662	0.7840	0.7698
	3	0.8010	0.7934	0.8170	0.8106
	4	0.8324	0.8292	0.8344	0.8210
	5	0.8963	0.8714	0.8570	0.8359
TH5	2	0.7401	0.7238	0.7419	0.7361
	3	0.8007	0.7952	0.7739	0.7680
	4	0.8591	0.8470	0.8255	0.8137
	5	0.8729	0.8667	0.8996	0.8811
TH6	2	0.7287	0.7207	0.7676	0.7533
	3	0.7728	0.7702	0.8272	0.8158
	4	0.8421	0.8388	0.8310	0.8237
	5	0.8899	0.8890	0.8485	0.8442

2	0.7009	0.6941	0.7920	0.7823
3	0.7765	0.7507	0.8189	0.8153
4	0.8461	0.8422	0.8335	0.8266
5	0.8914	0.8884	0.8628	0.8445
2	0.7194	0.6839	0.7921	0.7907
3	0.8192	0.8119	0.8213	0.8177
4	0.8476	0.8426	0.8418	0.8356
5	0.8777	0.8701	0.8550	0.8521
	$ \begin{array}{r} 2 \\ 3 \\ 4 \\ 5 \\ 2 \\ 3 \\ 4 \\ \end{array} $	3         0.7765           4         0.8461           5         0.8914           2         0.7194           3         0.8192           4         0.8476	3         0.7765         0.7507           4         0.8461         0.8422           5         0.8914         0.8884           2         0.7194         0.6839           3         0.8192         0.8119           4         0.8476         0.8426	3         0.7765         0.7507         0.8189           4         0.8461         0.8422         0.8335           5         0.8914         0.8884         0.8628           2         0.7194         0.6839         0.7921           3         0.8192         0.8119         0.8213           4         0.8476         0.8426         0.8418

#### 5.3 Results of HHO-CS algorithm using Otsu' betweenclass variance

Segmented results of HHO-CS algorithm using Otsu's method is shown in Figure 6. Both the low contrast and high contrast visual features are retained. The quality of the output is implicit. The proposed method may attract radio physicists to use it as an additional tool for diagnosis.

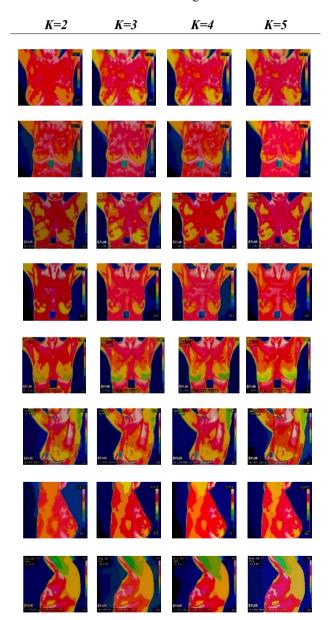


Figure 6. Results of HHO-CS algorithm using Otsu's method

#### 5.4 Experiment 2: Based on Kapur's entropy

Optimal threshold values, obtained using HHO-CS algorithm, are displayed in Table 7. Objective function values and PSNR values obtained from HHO-CS and HHO methods

using Kapur's entropy are presented in Table 8. Profound differences are seen. It is observed that the suggested HHO-CS method performs better than the HHO. Similarly, a significant improvement over the HHO algorithm is seen with respect to the PSNR values. The reason could be the enhanced exploitation capability of HHO-CS algorithm to achieve the

best solutions. Our method has shown consistently better PSNR values than HHO (see Table 8). The SSIM and FSIM values obtained from HHO-CS and HHO algorithms using Kapur's entropy are shown in Table 9. Interestingly, our method has shown better values (for the SSIM and FSIM) than the HHO.

Images	K		HHO-CS	
		R	G	В
TH1	2	227,234	42,179	233,252
	3	190,229,255	125,145,200	51,71,189
	4	132,137,187,247	15,104,136,210	32,42,141,233
	5	98,115,202,203,212	3,75,102,115,186	25,112,158,188,232
TH2	2	239,255	106,206	25,191
	3	208,235,255	16,132,247	35,88,238
	4	166,200,218,250	141,216,245,251	38,68,199,228
	5	116,153,168,190,250	98,103,177,200,215	42,60,80,176,198
TH3	2	221,227	230,239	186,255
	3	126,230,244	87,137,154	21,33,131
	4	129,156,204,223	80,84,187,227	126,190,222,227
	5	104,138,143,228,255	54,82,130,169,223	16,36,58,205,238
TH4	2	227,255	47,120	169,255
	3	137,158,236	82,121,254	62,120,190
	4	136,194,209,224	51,57,80,249	41,46,144,182
	5	164,166,239,245,254	5,51,59,114,118	85,164,176,187,20
TH5	2	236,249	87,254	44,148
	3	189,203,255	31,229,244	191,219,233
	4	188,202,219,253	115,147,239,250	3,40,132,252
	5	99,160,176,197,250	49,82,124,231,250	70,85,109,133,226
TH6	2	212,229	45,117	119,245
	3	137,168,203	115,129,218	3,73,153
	4	105,123,200,250	77,92,138,250	74,133,136,252
	5	147,196,209,230,252	19,35,66,133,164	36,69,188,222,243
TH7	2	250,252	179,242	178,243
	3	215,220,254	3,102,158	126,150,157
	4	104,184,237,246	33,49,156,208	5,68,117,245
	5	150,151,200,209,251	25,159,180,196,229	9,31,34,106,191
TH8	2	233,249	251,252	30,163
	3	219,225,233	14,142,219	69,100,124
	4	179,198,211,242	35,63,83,129	3,131,181,246
	5	89,139,166,202,234	26,79,102,114,251	27,34,74,149,159

Table 7. Threshold values of HHO-CS

# Table 8. Comparison of objective function values and PSNR obtained from HHO-CS and HHO algorithms using Kapur's entropy

		OBJECTIVI	E FUNCTION	PSN	R
Image	K	HHO-CS	ННО	HHO-CS	HHO
TH1	2	25.3967	23.8390	48.8151	48.3047
	3	36.4699	34.0063	53.1784	52.8795
	4	42.8620	39.4868	55.0468	54.5950
	5	50.2350	48.4930	59.3109	58.2001
TH2	2	25.8282	25.6571	53.1854	52.9000
	3	32.0311	31.2724	58.6532	58.1990
	4	40.5143	40.2226	62.7254	62.0969
	5	50.2481	48.3490	65.2311	65.6008
TH3	2	26.7611	26.6938	50.1649	48.5777
	3	33.3907	32.1520	52.0191	51.0425
	4	41.5988	40.8171	56.6610	56.1281
	5	51.4126	50.8451	60.1033	59.7543
TH4	2	26.8261	23.7504	53.8566	52.0168
	3	32.5919	31.6829	56.3193	55.2586
	4	37.2682	37.0698	61.9640	61.7853
	5	46.2737	46.1896	65.6875	65.5550
TH5	2	27.6672	27.1914	50.1393	48.6514
	3	34.4082	34.3798	54.0606	53.9827
	4	40.0538	39.3762	58.6640	57.6439
	5	48.3672	47.7147	60.4075	59.3283

TH6	2	26.9100	23.9546	50.3106	46.0928
	3	35.6760	33.8006	53.5330	51.0713
	4	44.2570	40.7154	62.0879	55.1715
	5	50.4478	50.3543	63.5159	63.5070
TH7	2	25.7328	25.5387	50.1983	50.1500
	3	32.2351	32.1220	53.8161	53.1795
	4	41.8437	41.7025	58.3176	57.5759
	5	45.9847	45.5572	60.1012	59.5965
TH8	2	25.8521	25.4122	48.1895	47.3364
	3	33.2082	32.3197	53.7797	53.6042
	4	40.5836	39.5286	58.8640	57.9005
	5	49.3672	49.3606	63.8921	63.8803

**Table 9.** Comparison of SSIM and FSIM values from HHO-<br/>CS and HHO algorithms using Kapur's entropy

		SSIM		FSIM	
Image	K	HHO-CS	HHO	HHO-CS	HHO
TH1	2	0.6241	0.5798	0.6870	0.6632
	3	0.6707	0.6643	0.7283	0.7103
	4	0.8155	0.8028	0.7510	0.7496
	5	0.8571	0.8317	0.7849	0.7835
TH2	2	0.5481	0.4899	0.7122	0.7084
	3	0.7343	0.6783	0.7438	0.7417
	4	0.7836	0.7482	0.7630	0.7583
	5	0.8283	0.8315	0.7782	0.7992

TH3	2	0.5980	0.5208	0.6772	0.6623
	3	0.7112	0.6878	0.7294	0.7228
	4	0.7358	0.7033	0.7668	0.7655
	5	0.8388	0.8058	0.7705	0.7765
TH4	2	0.5191	0.5160	0.7124	0.7100
	3	0.7289	0.6951	0.7456	0.7425
	4	0.7478	0.7266	0.7621	0.7617
	5	0.8016	0.7959	0.7926	0.7878
TH5	2	0.6818	0.5718	0.6790	0.6773
	3	0.7089	0.6686	0.7141	0.6978
	4	0.7416	0.7132	0.7284	0.7165
	5	0.8283	0.8208	0.7311	0.7298
TH6	2	0.4988	0.4164	0.7221	0.6941
	3	0.6538	0.5617	0.7579	0.7565
	4	0.7238	0.6815	0.7994	0.7879
	5	0.7364	0.7157	0.8185	0.8237
TH7	2	0.4523	0.4510	0.7920	0.7823
	3	0.6513	0.5336	0.8193	0.8189
	4	0.7897	0.6850	0.8335	0.8266
	5	0.7911	0.7208	0.8628	0.8445
TH8	2	0.4331	0.3654	0.7909	0.7921
	3	0.6004	0.4711	0.8213	0.8177
	4	0.7162	0.5864	0.8418	0.8356
	5	0.7819	0.6146	0.8550	0.8521

5.5 Results of HHO-CS algorithm using Kapur's entropy

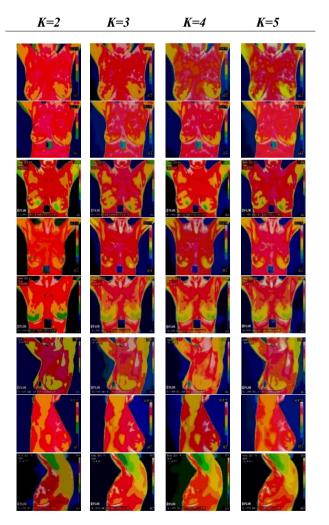


Figure 7. Results of HHO-CS algorithm using Kapur's entropy

Segmented results of HHO-CS algorithm using Kapur's entropy is shown in Figure 7. Both the low contrast and high contrast visual features are retained.

From this study, it is believed that the 1D Otsu's between class variance method outperforms 1D Kapur's entropy based technique. Because, infrared images, mostly have low contrast features. Therefore, between class variance helps us to compute optimal threshold values for separating different classes. It seems that the between class variance information is more than the entropy information in thermograms. In summary, the suggested multilevel colour image thresholding technique is useful for thermogram image analysis.

#### 6. COCLUSIONS

Unlike early multilevel thresholding method reported in the breast thermogram analysis, based on the gray-level images, the suggested method uses R, G, B colour components. The suggested technique is useful for the breast thermogram analysis. Results using the colour images may assist the clinicians, as an extra support, in the breast thermogram analysis. Nevertheless, the proposed HHO-CS optimizer helps us to compute optimal values for colour image thresholding. The exploitation capability of the HHO is enhanced, because the exploitation feature of CS is integrated in the system. Profound differences are observed while studying the convergence curves presented in this paper. The suggested HHO-CS performs better than both the HHO and CS optimizers. The speed of convergence is implicit (see Figure 3). The method has shown its ability to extract both the low and high resolution visual features, because all three colour components are used. The quality of the visual results is explicit (from Figure 6, 7). From Tables 4-6, it is observed that the RGB components based thresholding method using Otsu's objective function is better than the Kapur's entropy based approach; the reason is that the former fitness function could preserve more details. Therefore, the suggested RGB component based method using Otsu's between class variance may be suitable for pathological investigations. To figure out other merits, our method is faster and more accurate. It is reiterated that the proposed technique may attract the use of low cost and portable infrared cameras for analysis of breast thermograms. The proposal would be useful for analysis of other infrared images together with a clinical study. It is also believed that the suggested HHO-CS optimizer would be useful for function optimization to solve real world engineering problems.

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